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AFWAL-TR-81-3162 Part I



F-111E FLIGHT VIBRATION AND ACOUSTICS TEST

PROGRAM

PART I TEST INSTRUMENTATION, TEST PROCEDURE AND DATA REDUCTION

Structural Vibration Branch Structures and Dynamics Division

April 1982

Final Report for Period 25 July 1978 - 30 April 1981

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| A comprehensive test program was conducted on an F-1 | |
| of collecting dynamics data, primarily vibration and | acoustic data, at selected |
| locations throughout the aircraft under test conditions of the aircraft. Data were recorded from 1 | ions within the operational |
| phones at 60 test conditions including gunfiring pas | iss accelerometers and micro- |
| lengine parameter data were also recorded. The test | program is documented by pre- |
| senting the details on the test instrumentation, tra | ansducer locations, test pro- |
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20. ABSTRACT (Continued)

rmean square (RMS) levels which give a coarse indication of the dynamics environment of the F-111E. Detailed test results will be presented in the parts of this report which will follow.

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FOREWORD

This report documents an in-house effort conducted by the Structural Vibration Branch, Structures and Dynamics Division, Flight Dynamics Laboratory, Air Force Wright Aeronautical Laporatories, Wright-Patterson Air Force Base, Ohio.

This investigation was conducted under Flight Dynamics Laboratory Project 2401, Vibration Prediction and Control, Measurement and Analysis, Work Unit 24010401, Dynamics Environment on Current and Future Air Force Flight Vehicles.

The test aircraft was provided by 3246th Test Wing, Eglin Air Force Base, Florida, Mr. R. White (3246th TW/TETT) was the focal point for the test program conducted at Eglin Air Force Base during the July 1978 - September 1980 time period. The test support was provided by the 3246th TW under Test Number 1472TAO2, Support of AFFDL F-111 Vibration/Acoustic Testing. AFWAL/FIBG personnel who had primary responsibility for the test program were Messrs D. E. Seely and E. R. Hotz. Other personnel who made major contributions to the success of this effort were Messrs R. D. Talmadge, C. N. Willhite, J. E. Huffman and L. P. Vaughn. Special acknowledgment is due Mrs. Diana Howdyshell for typing the manuscript.

This report is Part I of a planned number of parts concerned with the F-111E flight test program. Part I presents the details of the test program with test results presented only to give an indication of data trends and data quality. The parts to follow will deal primarily with the spectral and statistical analysis of the recorded data.

This report was released for publication by the authors in August 1981.



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SECTION I

INTRODUCTION

One of the most severe problems in airborne equipment design, application, testing, and use is the lack of sufficient data to define the actual dynamic environment under which equipment in the vehicle must operate. In most cases, this lack of data has resulted in: (1) overdesigning the equipment which results in excessive cost, size and weight or (2) underdesigning the equipment with a resulting lack of reliability and limited service life. This problem is even more acute in designing both equipment and structures used in high speed aircraft which must operate in a severe dynamics environment.

To alleviate this deficiency, the Structural Vibration Branch, Structures and Dynamics Division, Flight Dynamics Laboratory, has implemented a comprehensive data acquisition program aimed at obtaining vibration and acoustic data on all available aircraft.

This report describes the flight test program conducted on an F-111E aircraft. The purpose of this program was to collect dynamics data, primarily vibration and acoustics data, at selected locations throughout the aircraft under test conditions within the operational envelope of the aircraft.

Additional data including temperature, pressure, air flow rate, and humidity were also collected. The purpose of this report is to document the test program by presenting the details of the test instrumentation, transducer locations, test procedures, and flight conditions. Test results are limited to overall and peak root mean square (RMS) levels which give a coarse indication of the dynamics environment of the F-111E. It is intended that this report be used primarily for selecting transducers and test conditions requiring more detailed data reduction. Detailed test results will be presented in the parts of this report which will follow.

SECTION II

DESCRIPTION OF TEST VEHICLE

The F-111E aircraft, manufactured by the Fort Worth Division of General Dynamics, is a two-place, all-weather, high or low altitude, supersonic, tactical fighter bomber. The aircraft has dual controls and requires a crew of two, seated side-by-side. The aircraft provides the pilot with the in-flight capability to select any angle of wing sweep between 16 and 72.5 degrees. The aircraft has full-span fowler action, double slotted trailing edge flaps, and is powered by two TF30 fan jet afterburning engines internally mounted in the fuselage. The aircraft has a conventional tricycle gear with the main gear as a single assembly. The aircraft has a large vertical stabilizer and a conventional rudder plus ventral strakes located on the lower portion of the engine access doors approximately 30 degrees from the vertical.

The F-111E aircraft used for the test program was Tail Number 68-058. During the period 5 Oct 79 to 18 Sep 80, there were 37 test flights. On each test flight, the aircraft was configured to collect dynamics data for various combinations of internal and external stores. The internal stores included an M61 20MM cannon which was fired on nine of the flights. The aircraft was also flown with two types of experimental fluctuating pressure suppressors (spoilers) installed forward of the weapons bay and a slanted ramp installed in front of the rear bay wall. These devices were being tested to determine their effectiveness in reducing noise in the weapons bay when the bay doors were open.

SECTION III

TEST INSTRUMENTATION

The airborne data acquisition system is shown in block diagram in Figure 1. The system used 104 accelerometers and 29 microphones to measure the vibration and acoustic environment of the aircraft. The type and characteristics of the transducers used to measure acceleration and sound pressure level are summarized in Table 1. In addition to dynamic transducers (accelerometers and microphones), the system used 15 thermocouples, two airflow sensor systems, a humidity sensor, and a pressure transducer to measure slower varying aircraft characteristics. These transducers are summarized in Table 2. In addition, the total instrumentation system included: (1) an in-house fabricated programmable transfer box; (2) a 12-position Legex, Inc. switch box; (3) a Master six-channel automatic gain changing (AGC) amplifier box; (4) a Secondary sixchannel AGC amplifier box, (5) a pair of frequency multiplexers (Microcom Corp. Micromount Model MM402-10) each consisting of two voltage controlled oscillators (VCO) and one mixer amplifier with respective VCO center frequencies and deviations of 128 KHz + 16 KHz (+2.5V) and 176 KHz + 16 KHz (+2.5V): (6) a Mars 2000 Tape Recorder; (7) a Base Ten, Inc. Portable Data Acquisition System (PDAS) Data Collector; (8) a time code generator; and (9) voice from the aircraft intercom system.

A complete listing of all transducer identification numbers, locations, and types is contained in Table A-1. Overall transducer locations are illustrated in Figure 2. Figures A-1 thru A-6 are more detailed drawings showing transducer locations. Figure A-7 cross references the transducer number with the Figure numbers (A-8 - A-81) of the photographs which show the precise transducer locations.

Where possible, accelerometers were mounted by using double sided #10-32

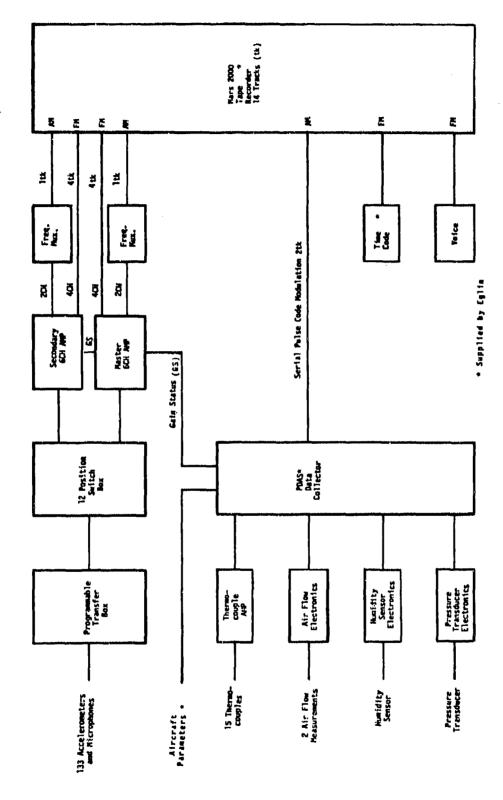


Figure 1. Data Acquisition System

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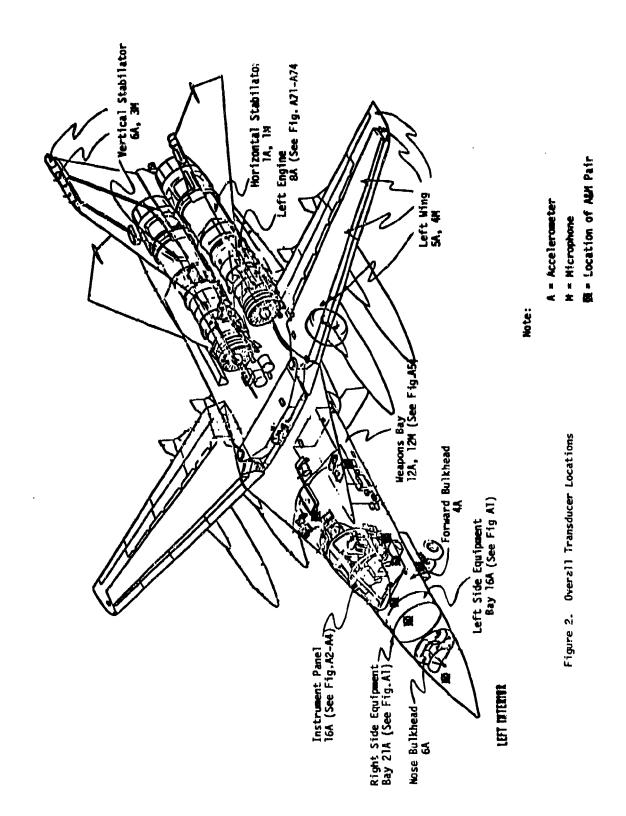
TABLE 1

VIBRATION AND ACOUSTIC TRANSDUCERS

| FREQ. RESPONSE (100 Megohns Load) | 1HZ- 6KHZ 1HZ- 6KHZ 2HZ- 6KHZ (+5%) 25HZ- 5KHZ (+5%) 2HZ-10KHZ (+3d8) |
|--------------------------------------|---|
| NOMINAL | 10mvp/gpk 10mvp/gpk 10mvp/gpk 10mvp/gpk 32mvrms/ 140d8SPL |
| (pfd) | 8,000 8,000 10,000 3,500 |
| TEMP RANGE | -65 F to 300 F -65 F to +500 F -65 F to +350 F -320 F to +750 F -100 F to ∓300 F |
| QUAN- | 68 17 14 5 29 133 |
| MODEL | 902-H 902-HT 2215 2245 MVA-2100 (5/8") |
| TRANSDUCER TYPE | Columbia Crystal Accelerometer Columbia Crystal Accelerometer Endevco Crystal Accelerometer Endevco Crystal Accelerometer Gulton Piezoelectric Microphone |

TABLE 2 PDAS TRANSDUCERS

| COMMENTS | | Not operational due to improper installation | | | | | | |
|-----------------|---|--|--|---|---------------------|------------------------------|------------------|--|
| RANGE | Programable | -65 F-150 F 1#/s-10#/s | 0%-100% | -30 C-50 C | 30"Hg-3"Hg | -10db to 60db | 1-12 | |
| VALUES | -1.25V to +3.25V | +20mvdc 0-5VDC | 0-10VBC | 3V5V | 0-5YDC | +2.5VDC | 0-5VDC | |
| NO. SIGNALS | 15 | 00 | н | H | Н | 21 | - | æ |
| SIGNALS | Temperature | Air-flow Temperature Air-flow Reading | Relative Humidity | Relative Humidity Temperature | Absolute Pressure | AGC Gains | Switch Position | |
| TRANSDUCER TYPE | Type J (Iron-Constan- tan) Thermocouples | Rosemount Model 519CVI-Air Flow Measurement System | Thunder Scientific, Hamidity Sensor | Signal Conditioner Model SC-200C-H1-T11 Sensing Element Model BR-101B-LT | Pressure Transducer | AGC Amplifier Commutator Out | Switchbox, Ledex | Eglin-Supplied Aircraft Parameters |



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insulated mounting studs. One side of the stud attached to the accelerometer and the other side attached to drilled and tapped holes in the structure. A single sided stud was used where holes were not allowed. The flat side of the stud was glued to a clean and sanded surface of the structure using Eastman 910 cement and the #10-32 side was attached to the accelerometer. Most of the microphone brackets were installed using a special glue formulated by Eglin personnel. Some of the microphones were installed by drilling and tapping holes to match the microphone bracket mounting holes. All external microphones were flush mounted where possible. Thermocouples which sensed structural temperatures were attached to the surfaces with epoxy. Thermocouples measuring air temperature were suspended in the air. Specific information concerning transducer mounting can be obtained from the photographs in Figures A-8 - A-81.

Each microphone and accelerometer was calibrated in the Laboratory by AFWAL/FIBG to obtain sensitivity and frequency response characteristics. After installation and prior to the initial test flight, the accelerometers were calibrated end-to-end by inserting a known calibration signal at the transducer end of the system and recording the resultant electrical signal on tape. The microphones were calibrated by applying a precise 124dB SPL to each microphone with a Bruel & Kjaer Instruments, Inc. type 4220 Pistonphone and recording this resultant electrical signal on tape. The system calibration was then determined in the Laboratory using the calibration tape.

The complete listing of PDAS input signals is given in Table C-1. In addition to the temperature, airflow, humidity, and pressure sensors mentioned earlier, the PDAS accepted aircraft parameters supplied by other aircraft systems and recorded simultaneously with the signals from transducers. The PDAS Data Collector time division multiplexed all the input signals shown in Table C-1. The system digitally encoded each data sample to a 10 bit binary word which was then converted into a serial pulse code modulation output. The

PDAS system output was 80 k bits/second. The gain status codes from each of the 12 AGC amplifiers and switch position code were also multiplexed by the PDAS.

The signal leads from the 133 accelerometers and microphones were assigned i to the 144 inputs of the switch box by the Programmable Transfer Box. Six of the signal leads were paralleled to two or more switch box input slots. The Ledex, Inc. Switch Box had 12 switch positions with 12 signals output for each position of the switch. This permitted switching through 144 input signals 12 at a time. For example, switch position 1 switched in input slots 1-12, switch position 2 switched in input slots 13-24, and so forth. The AGC amplifiers would automatically change gain to provide an optimum input signal level for the recorder and multiplexers. In addition, each amplifier had a gain status output which was a DC level that identified the gain level. These 12 gain status signals were input to the PDAS system. Eight amplifier signals and two frequency multiplexed outputs were then input to the tape recorder as shown in the block diagram (Figure 1). Thus, 4 of the 12 amplifier outputs were frequency multiplexed into 2 tape tracks as shown in the block diagram (Figure 1). Frequency modulation (FM) recording with a center frequency of 54 KHz (Wide Band I) was used for the amplifier outputs, and amplitude modulation (AM) recording was used for the frequency multiplexer and PDAS outputs. Table A-2 shows the transducer ID, tape track (channel), and switch position assignments.

The accuracy limitations of the flight measurement system were due to error contributions from the transducers, signal conditioning equipment, and tape recorder. The maximum error of any one of these elements is unlikely to exceed ± 5% of full-scale output. A reasonable estimate of maximum likely overall error is the root-mean-square of the errors from the three contributors or 8.7% of full-scale output.

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SECTION IV

TEST PROCEDURE

Dynamics data were recorded for test conditions which included ground runup, takeoff, climb, level acceleration and deceleration runs, sideslips, turns, stabilized flight, gunfiring passes, landing, and standard maneuvers. A complete listing of these test conditions including Mach numbers and altitudes is given in Tables 3 and 4. The test conditions listed in Table 4 are more of a transient nature, while those listed in Table 3 are for stabilized flight.

The test coordinator was initially provided a list of the desired flight test conditions. From this list, the test pilot selected the specific test conditions to be flown on each flight or mission. The initial missions concentrated on acquiring data samples throughout the aircraft flight envelope and identifying maneuvers that resulted in higher vibration/acoustic environments.

During a stabilized flight condition, data were recorded simultaneously for 12 transducers that were grouped together on one switch position. The switch was then advanced to the next position and data were recorded for the second set of 12 transducers while the pilot maintained the same stabilized flight condition. This procedure continued until the switch had been sequenced through all 12 positions and data had been recorded for all 133 accelerometers and microphones. Several of the accelerometers and microphones were paralleled onto two or more switch positions in anticipation of a need for time correlation with transducers on these other switch positions. Typical data samples were 20 seconds.

For the flight test conditions which were of a transient nature, (e.g., takeoff, acceleration and deceleration runs, and maneuvers), it was necessary to repeat each test condition for each of the switch positions. In these cases, the tape recorder was turned on just prior to performing the test condition and shut off at completion of the test condition. This resulted in test records in some cases of 3 to 5 minutes in duration. It should be noted that all of the data input to the PDAS

TABLE 3
TEST CONDITIONS PRODUCING FLAT RMS AMPLITUDE RESPONSE AS A FUNCTION OF TIME

| Test Condition Number | Mach Number | Altitude (K Ft) | Test Condition |
|-----------------------------|----------------|--------------------|---|
| 7 | .85 | 3 | Steady heading sideslip |
| 8 | .85 | 3 | Level turn, constant G |
| 17 | .60 | 3 | Stabilized level flight |
| 18 | .70 | 3 | Stabilized level flight |
| 19 | .80 | ž | Stabilized level flight |
| 20 | .90 | 3 3 | Stabilized level flight |
| 21 | 1.00 | 3 | Stabilized level flight |
| 22 | .80 | 15 | Stabilized level flight |
| 23 | .90 | 15 | Stabilized level flight |
| 24 | 1.00 | 15 | Stabilized level flight |
| 25 | 1.20 | 15 | Stabilized level flight |
| 27 | .90 | 30 | Stabilized level flight |
| 28 | 1.00 | 30 | Stabilized level flight |
| 29 | 1.20 | 30 | Stabilized level flight |
| 57 | .7 | 17 | MSL instrumentation check |
| 60 | .62 | - 3 | Gunfire (4 seconds), altitude - level |
| 61 | .65 | 15 | Gunfire (4 seconds), altitude - 10 degree |
| 01 | | | dive |
| 62 | .6 8 | 10 | Gunfire (4 seconds), altitude - 10 degree |
| V- | | | dive |
| 63 | .92 | 30 | Gunfire (4 seconds), altitude - 10 degree |
| | | | dive |
| 64 | .73 | 15 | Gunfire (4 seconds), altitude - 10 sgree |
| • • | | | dive |
| 65 | .92 | 30 | Gunfire (4 seconds), altitude - 15 degree |
| • • | | | dive |
| 66 | .68 | 15 | Gunfire (4 seconds), altitude - 20 degree |
| | | | dive |
| 67 | .80 | 13 | Gunfire (4 seconds), altitude - 30 degree |
| | | | dive |
| 78 | | | Weapon carriage |
| 83 | .75 | 10 | Stabilized level flight |
| 84 | .60 | 5 | Stabilized level flight |
| 85 | .70 | 8 | Stabilized level flight |
| 86 | .60 | 10 | Stabilized level flight |
| 87 | .70 | 10 | Stabilized level flight |
| 88 | .75 | 15 | Stabilized level flight |
| 89 | .70 | 15 | Stabilized level flight |
| 90 | .78 | 3 | Stabilized level Clight |

TABLE 4

TEST CONDITIONS PRODUCING VARYING RMS AMPLITUDE RESPONSES AS A FUNCTION OF TIME

| Condition Number | Mach Number | Altitude (K Ft) | Test Condition |
|---------------------|----------------|--------------------|--|
| 1 | | | Ground run, taxi prior to takeoff |
| 1 2 4 | | | Ground run, taxi after landing |
| 4 | | | Takeoff from engine run-up to 15 seconds after liftoff |
| 5 | | | Landing, 20 seconds before to 15 seconds |
| | | | after touchdown |
| 9 | .85 | 3 | Level turn, Max G |
| 12 | 1.0550 | 3 3 | Standard maneuver #3, level deceleration |
| *= | 1100 100 | • | (Speed Brakes Out) |
| 13 | | | Standard maneuver #4, aerobatics |
| 14 | .4-1.05 | 3 | Level acceleration |
| 15 | .5-1.2 | 15 | Level acceleration |
| 16 | .75-1.3 | 30 | Level acceleration |
| 38 | 1.14 | 30 3 | Deceleration, weapons bay open |
| 39 | 1.25 | 15 | Deceleration, weapons bay open |
| 40 | 1.37 | 30 | Deceleration, weapons bay open |
| 41 | 1.045 | Š | Deceleration, weapons bay open |
| 42 | 1.04 | 5 3 | Deceleration, weapons bay closed |
| 43 | 1.245 | 15 | Deceleration, weapons bay closed |
| 44 | 1.37 | 30 | Deceleration, weapons bay closed |
| 50 | .5-1.12 | 17K | Level acceleration |
| 51 | .9-1.13 | 15 | Speed dash, missile on |
| 53 | 1.07-1.25 | 30 | Speed dash, missile on |
| 55 55 | .98-1.1 | 35 | Speed dash, missile and camera on |
| 56 | .9-1.1 | 8 | Speed dash, missile and camera on |
| 79 | | 12 | |
| /9 | 1.1 | 14 | Weapon release |

(e.g., thermocouple, flight parameters and amplifier gains) were recorded anytime the tape recorder was switched on.

The slow (3-5 minute) aircraft acceleration runs from minimum to maximum Mach numbers at several altitudes were made to allow structural resonances which might be present to build to a peak. These resonances could well occur at Mach numbers for which no stabilized data were to be recorded. When a possible resonance was indicated in playback of the data, the Mach number and altitude for this resonance were determined and a request made to fly this condition in a stabilized test condition.

An operational restriction on the aircraft prohibited acceleration runs with the weapons bay doors open. Therefore, deceleration runs from maximum to minimum Mach number at different altitudes were made with the weapons bay doors open. The following bay configurations were tested:

- (1) Empty
- (2) With M61 20MM cannon installed
- (3) With M61 and BDU-8 installed
- (4) With two BDU-8s installed
- (5) With and without modifications (spoilers in front of bay and slanted ramp at rear of bay)

A total of 37 records of data were recorded during gunfire passes where 14,000 rounds of ammunition were fired by a M61 20MM cannon mounted in the right weapons bay. Each gunfiring pass consisted of 3-4 seconds of continuous firing at a rate of 100 rounds/second. A 2.5 minute waiting period was required between firings for gun cooling time.

On nine of the test flights, the aircraft was carrying either two or four external stores on the wing pivot pylons. The stores included the GBU 10C/B, MK84 and the CTU-2. External stores were released on some of the flights.

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Table A-3 relates weapons bay configuration, external store configuration, and M61 gunfiring records with particular flight mission numbers.

SECTION V

DATA REDUCTION AND PRESENTATION

Data tapes recorded on each test flight were copied and sent to AFWAL/FIBG for data reduction. Figure 3 shows a block diagram of the system used to accomplish the playback and processing of the FM, AM, pulse code modulation (PCM), and frequency multiplexed data contained on each test tape. The primary purpose of this initial data reduction was to quickly assess the quality of the recorded data in order to identify any flight instrumentation problems which required correction prior to continuing with the flight test program. This approach for identifying and correcting instrumentation problems aided in improving overall data quality. Approximately 86% of the data are a naidered usable.

Each data tape was played back and reduced on the system shown in Figure 3. Six channels of data were reduced at a time; this required two passes through the tape to process all twelve channels of dynamics data. During each pass through the tape, six channels of data were stripped out on an oscillograph recorder at a paper speed of 0.1 inches per second with line code printed on the edge of the paper. These stripouts were used in correlating test conditions from the flight test card or log with the data actually recorded on tape. The oscillograph stripouts were also useful in determining the quality of the recorded data. Simultaneously while stripping out the data on the oscillograph each of the six analog data channels was also input to RMS detectors. The RMS detectors had a time constant of 230 milliseconds with a very flat frequency response as shown in Figure 4. The DC output of each RMS detector was input to an analog to digital conversion system simultaneously with the gain status of each AGC amplifier and the instantaneous time read from the time code tape track. These data were sampled at the lowest available digitizing rate of seven samples per second for each input channel. This rate provided more than adequate resolution and could have been lowered to 1 or 2 samples per input channel. This part of the data

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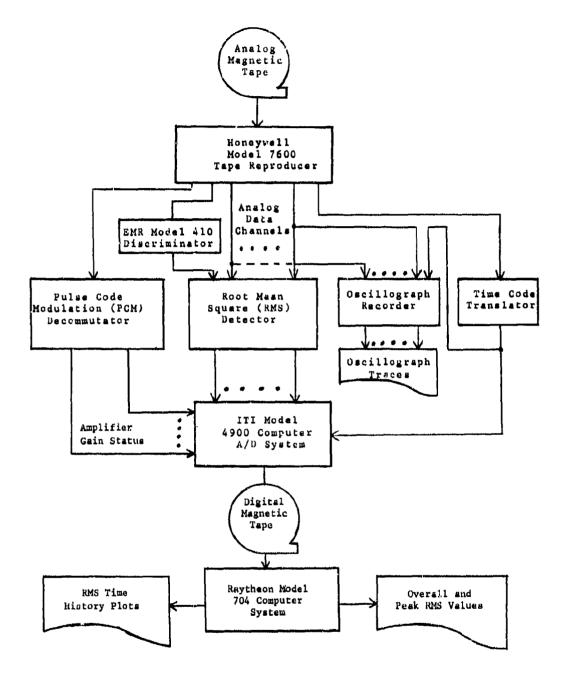


Figure 3. Data Playback and Reduction System

Companies and a

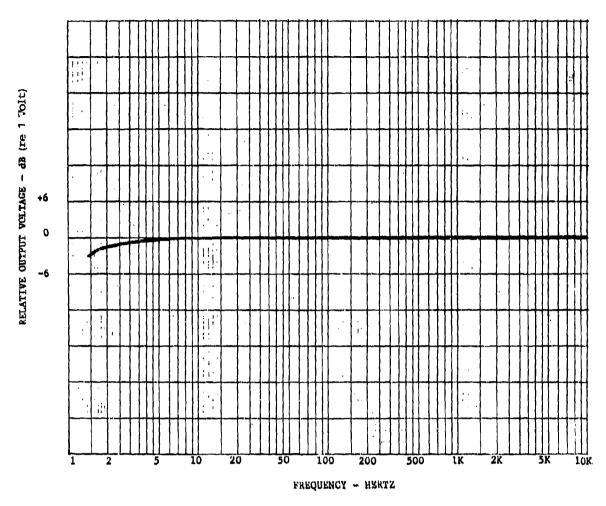


Figure 4. RMS Detector Frequency Response

reduction process was automated; therefore, once the system was set up, the flight tape could be played back in its entirety with no operator assistance required other than rewinding the tape and starting it for the second pass.

The digital tape produced by the analog to digital system was then input to a Raytheon Model 704 computer system along with transducer sensitivities and pickup identification (PUID) codes. Computer software then applied the proper amplifier gain factor and the matching transducer sensitivity to each data sample to produce RMS time history data in engineering units of G-PMS for accelerometer data and dB-sound pressure level for microphone data. Individual RMS time history plots were then made for each transducer for all test records. The initial time history plots revealed a need for additional smoothing to reduce the effects of transients in the data which were directly related to the data acquisition or reduction instrumentation. Examples of these are: a momentary loss of PCM decommutator synchronization signal, change of amplifter gain, and change of switch position. To overcome this problem, a "running average" technique was employed. This averaging technique simply replaced each data point with the average of its amplitude and the amplitude of some specified number of successive data points. It was determined that an eight-point running average produced the desired smoothing. Three typical time history plots are shown in Figure 5. A symbol plotted on the time history curve indicates that during the recording of the data. the signal level exceeded the set upper or lower level limits of the auto-gain ranging amplifier causing the amplifier to step up or down in gain to bring the data signal back into the optimum range of the tape recorder. Printed in the upper right corner of each plot is the initial amplifier gain level in dB (e.g., 40dB = X100 gain) and the actual start time of the record. Any gain change is printed below the starting gain along with the time of occurrence. This information is very useful in performing further data reduction. In addition, the overall RMS level which is computed over the entire test record is printed along

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Mission No. 1016, 19 May 80 Test Condition - 9: Left Turn, Max g, Mach 0.85 @ 3K feet

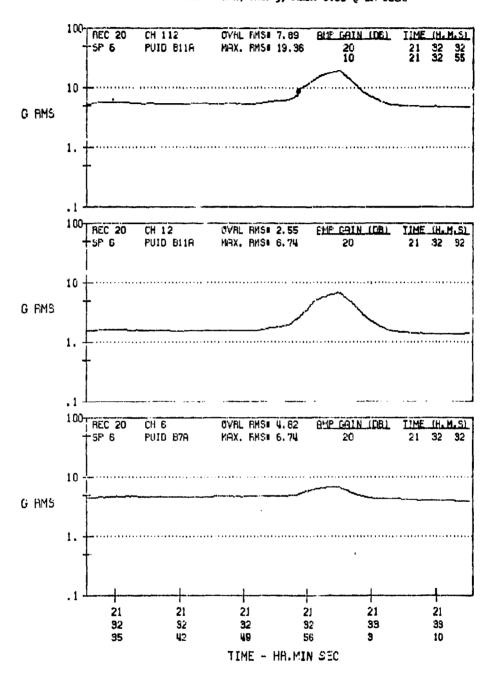


Figure 5 Typical RMS Time Histories

with the maximum RMS level attained during the test record.

Approximately 7200 individual time history plots were produced. Since it is not feasible to include that many plots in this report, it was decided to present this data in condensed but still usable form. About one-half of the time history plots exhibit a relative flat or constant amplitude. Figure 6 shows three typical examples of this type of time history. Data which exhibits this flat amplitude response with time can be represented by its overall RMS level. A list of flight conditions which produced relatively flat amplitude time history responses was given in Table 3. The overall RMS levels for transducer data recorded for these test conditions are given in Appendix B. Table B-1. This table contains the RMS data for each set of 12 transducers for each indicated switch position. In many cases, the same test condition was flown more than once. This is indicated in the tables by consecutive entries of the same test condition code. Time history plots which do not exhibit a flat amplitude level are produced by flight conditions of a transient nature. A list of these flight conditions was given in Table 4. Figure 7 shows three typical examples of time history plots with varying amplitude levels. For this type of data, the maximum amplitude which occurs within a given test record is of more value than the overall RMS. Appendix B, Table B-2 presents maximum RMS levels as read from the time history plots for each transducer.

Data which has been identified as unusable due to instrumentation problems is indicated in Tables B-1 and B-2 by an RMS amplitude of .00. These instrumentation problems were identified during the data editing phase of producing the RMS values. It is suspected that a limited amount of questionable data still remains to be identified. This questionable data probably represents less than 1-2% of the presented RMS data and will be identified during the future spectral analysis phase of data reduction. The spectral analyses will identify the frequency and amplitude of the complex responses which were summed

Mission No. 1012, 28 Apr 80

Test Condition - 23: Stabilized Level Flight, Mach 0.9 g 15K Feet

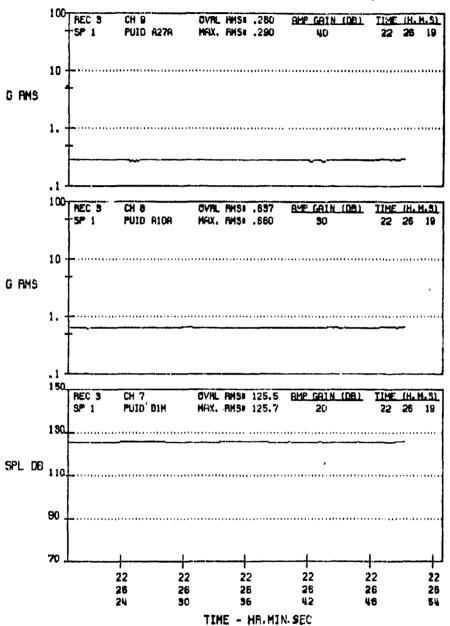


Figure 6 Typical Flat Amplitude RMS Time Histories

Test Condition - 15: Level Acceleration, Mach 0.5-1.05 @ 15K Nest 100 | REC 12 CH 5 OVAL AMS! 2.41 BMF GAIN (DB) TIME IH, J.SL FUID ROTA MAX. PMSI 4.85 40 30 20 17 47 19 6 16 26 SP 4 10 G RMS 1. REC 12 CH 3 OVAL AMS. 3.40 AMP CAIN (DR) PUID RIZA MAX. MMS# 6.41 10 G RMS 1. 100 | REC 12 CH 3 CVRL RMS# 1.04 BMP GRIN IDB1 PUID RIIR MAX. MMS# 2.27 10 G RMS i. 20 18 20 20 20 20 20 20 30 18 19 19 20 0 ٥ 30 30

Mission No. 3013, 30 Apr 80

Figure 7 Typical Varying Amplitude RMS Time Histories

TIME - HR. MIN. SEC

in the RMS process to produce each overall RMS amplitude level. This information will be presented in succeeding parts of this report.

Reduction of the large amount of data collected on the PCM channel has been limited to making computer listings of this data at one-second time intervals. These listings were provided by the Math Lab at Eglin AFB FL. Appendix C. Tables C-1 thru C-4 are reproductions of typical listings for each type of printout. These listings are available for later use in correlating aircraft measured dynamic response with flight parameters, temperatures, flow rates, etc.

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SECTION VI

PLANNED DATA ANALYSIS

The dynamics data measured on the F-111E will be used in several specific efforts now being conducted within the Air Force. These efforts are briefly described in the following paragraphs.

- 1. AFWAL/FIBG Work Unit 24010414. The title of this work unit is "Vibration Analysis and Testing Technology". A major part of this work unit is devoted to the development and verification of empirical methods for the prediction of both linear and angular vibration of aircraft structures. Much of the data measured on the F-111E will be used to improve and expand these existing prediction methods. The data will also be used to study a new prediction technique for vibration transmitted from external skin structure to internal compartment sub-structure and equipment. This will involve using measurements from pairs of accelerometers and microphones which were installed at specified locations throughout the F-111E aircraft.
- 2. AFWAL/FIBE Work Unit 24010146. The title of this work unit is "Acoustics Research". One area being studied under this work unit is internal weapons bay aero-acoustic environments. The internal weapons bay environment immediately before and during weapons release continues to present severe aircraft, weapons design, structural, and operational problems. A substantial part of the F-111E vibration and acoustics test program was conducted to measure the weapons bay aeroacoustic environment with the bay doors open with and without fluctuating pressure suppression devices installed. This measured data will be evaluated to determine effectiveness of the suppression devices in reducing the weapons bay aeroacoustic environment. Initial results of this effort were reported in Reference 2.
- 3. AFWAL/FIBG Work Unit 24010401. The title of this work unit is "Dynamics Environment on Current and Future Air Force Flight Vehicles". Overall

RMS vibration measurements will be modeled as the sum of a general mean plus a location effect plus a test condition effect plus an interaction constant times the product of these two effects. From these results, locations and test conditions for broad band spectral analyses will be selected. Then spectral magnitudes at each frequency will be modeled in the same way and the results plotted to show on the same graph, the same frequency spectrum of the general mean, the location effect, the test condition effect, and the interaction constant. These results can then, in turn, be used to determine the need for further narrow band analyses. Regression analyses will be employed to model the test condition effects as functions of airspeed, altitude, engine power, etc. Analyses of variance will be used to model location effects in terms of structural characteristics and direction. Factor analyses will also be used to determine the extent to which all spectral plots obtained can be modeled as linear combinations of a few more fundamental plots. This work will be reported in subsequent parts of this report.

4. TN-ASD-AFWAL-2011-75-17(01). The title of this technology need (TN) is "Updated Dynamics Qualification Test Criteria and Techniques" dated 17 Oct 80. The objective of this TN is to refine and augment the dynamic test methods of MIL-STD-810. One particular area to be updated is that which covers gunfire criteria. The gunfire vibration prediction method contained in the present version of MIL-STD-810 was developed prior to 1975. Gunfire data from the F-111E test program and from other recent test programs will be used to evaluate a recently developed simplified gunfire vibration prediction method. Vibration and acoustic data will also be made available for updating other sections of MIL-STD-810 as well.

SECTION VII

CONCLUSIONS

- 1. A large quantity of vibration and acoustic test data recorded throughout the operational flight envelope of the F-111E is now available for use in dynamics rosearch and development efforts, designing electronic and electro-optical systems, updating dynamics qualification test criteria, and solving present and future operational dynamics problems on the F-111E.
- 2. To improve the overall quality of dynamics test data on large flight test programs, it is essential that test tapes be played back and reviewed for quality following each test flight with adequate time provided to correct major instrumentation problems prior to continuing the flight test program. The use of an RMS Detector System and time history computer software provides an effective "quick look" method for determining the quality of flight test data.
- 3. The flight parameter data which was sampled and recorded along with the dynamics data was very useful in correlating aircraft performance with dynamics response. Much of the scatter in the dynamics data can be attributed to the difficulty in maintaining stable flight conditions over the length of test records and the necessity of setting up and repeating flight conditions for each set of 12 transducers.

APPENDIX A TRANSDUCER LOCATIONS AND AIRCRAFT TEST CONFIGURATIONS

| FIGURES | | | | | | |
|------------|---|--|--|--|--|--|
| A-1 | Accelerometer Locations in Nose Equipment Bay | | | | | |
| A-2 | Accelerometer Locations on Left Main Instrument Panel | | | | | |
| A-3 | Accelerometer Locations on Center and Right Main Instrument Panel | | | | | |
| A-4 | Accelerometer Locations on Center Console | | | | | |
| A-5 | Sketch of Accelerometer and Microphone Locations in Weapons Bay | | | | | |
| A-6 | Thermocouple Locations in Right Side Nose Equipment Bay | | | | | |
| A-7 | Cross Reference: Transducer Number with Figure Number of Photograph Showing Precise Transducer Location | | | | | |
| A-8 - A-81 | Photos of Transducer Locations | | | | | |
| TABLES | | | | | | |
| A-1 | Description of Transducer Locations | | | | | |
| A-2 | PUID/Channel/Switch Position Matrix | | | | | |
| A-3 | Aircraft Test Configurations | | | | | |

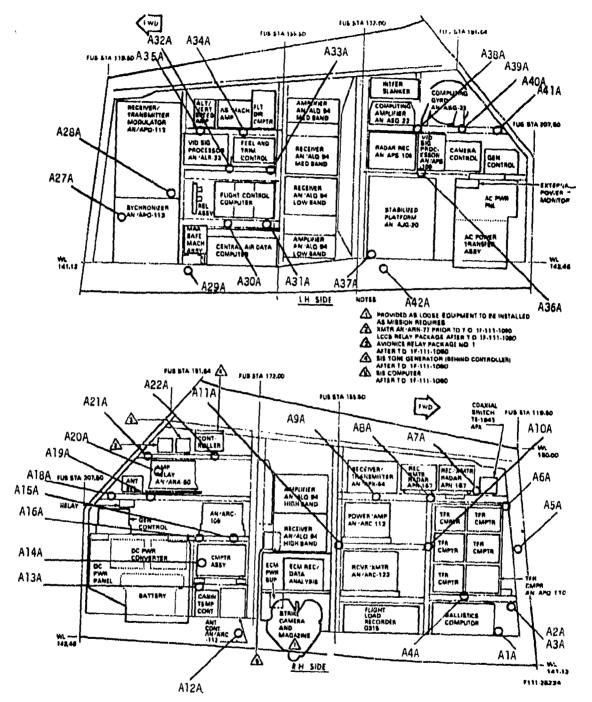


Figure A-1 Accelerometer Locations in Nose Equipment Bays

and a second view of the

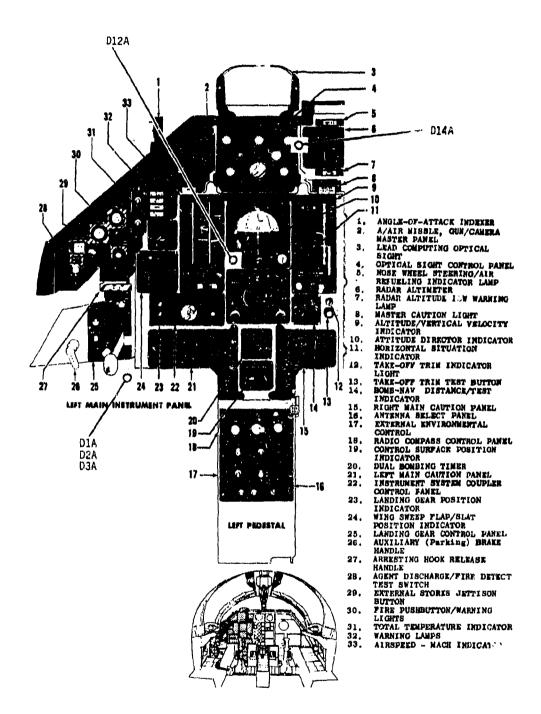


Figure A-2 Accelerometer Locations on Left Main Instrument Panel

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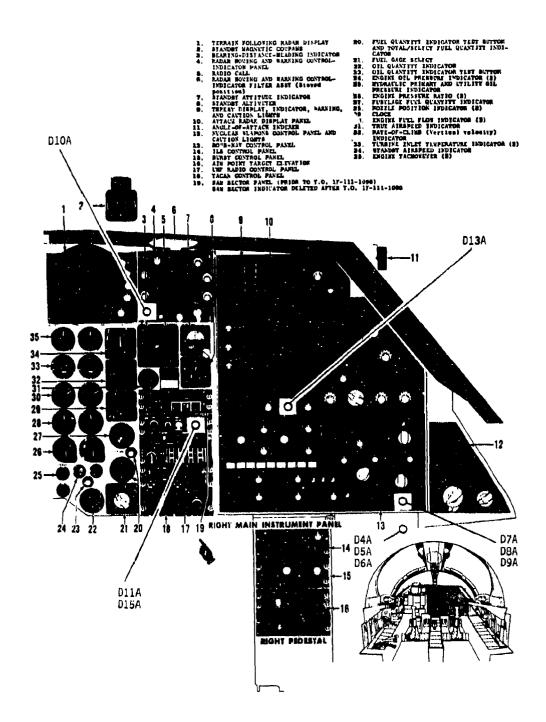


Figure A-3 Accelerometer Locations on Center and Right Main Instrument Panel

4

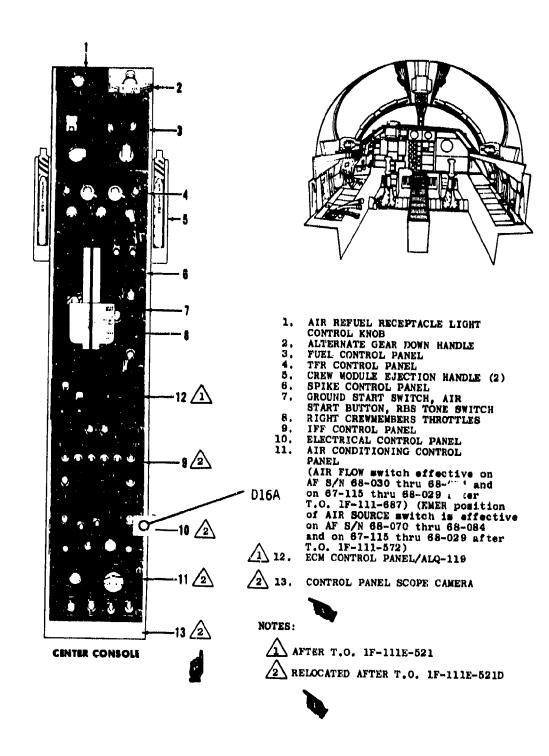
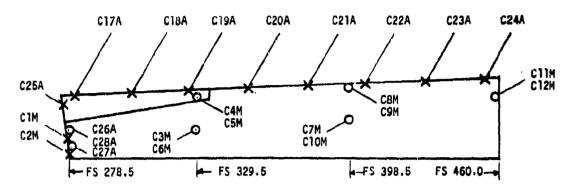


Figure A-4 Accelerometer Locations on Center Console

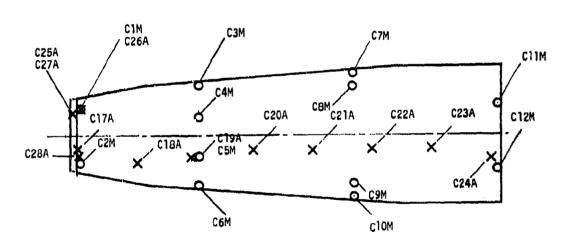
COLUMN TO STATE OF THE STATE OF



SIDE VIEW

X - ACCELEROMETER

O - MICROPHONE



BOTTOM VIEW

Figure A-5 Sketch of Accelerometer and Microphone Locations in Weapons Bay

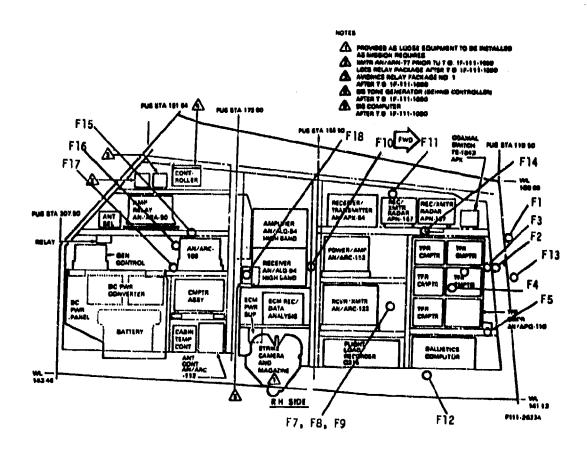


Figure A-6 Thermocouple Locations in Right Side Nose Equipment Bay

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| TRANSDUCER NUMBER | FIGURE NUMBER | TRANSDUCER NUMBER | FIGURE NUMBER | TRANSDUCER NUMBER | FIGURE NUMBER |
|---|--|---|--|--|---|
| NUMBER A1A A2A A3A A4A A5A A6A A7A A8A A11A A11A A11A A11A A11A A11A | NUMBER A-8, A-9 A-8, A-9 A-8, A-9 A-8, A-9 A-10 A-8, A-11 A-8, A-11 A-8, A-11 A-8, A-12 A-8, A-12 A-8, A-14 A-8, A-14 A-8, A-14 A-8, A-14 A-8, A-15 A-8, A-17 A-16, A-17 A-16, A-18 | NUMBER A33A A34A A35A A36A A37A A38A A39A A40A A41A A42A A44A A44A A44A A44A A45A A44A A45A A46A A47A A48A A49A A51A B2A B1A B2A B3A | NUMBER A-16, A-19 A-16, A-19 A-16, A-20 A-16, A-20 A-16, A-20 A-16, A-20 A-16, A-20 A-16, A-21 A-22 A-22 A-22 A-23 A-24 A-25 A-26 A-26 A-26 A-28 A-29 A-30 A-32 | B8A B9A B1OA B11A1 B11A2 B12A B13A B15A B16A B1M B2M B3M B4M B3M B4M B5M B6M B7M B8M B10M B13M B13M B13M B13M B15M | NUMBER A-36 A-37 A-38 A-38 A-39 A-40 A-41 A-42 A-43 A-27 A-29 A-30 A-31 A-32 A-33 A-34 A-35 A-36 A-37 A-38 A-39 A-40 A-41 A-42 |
| A30A A31A A32A | A-16, A-18 A-16, A-18 A-16, A-19 | B5A B6A B7A | A-34 A-34 A-35 | B16M C1M C2M C3M | A-43 A-46, A-47 A-47 A-48 |

Figure A-7 Cross Reference: Transducer Number with Figure Number of Photograph Showing Precise Transducer Location

| TRANSDUCER NUMBER | FIGURE NUMBER | TRANSDUCER NUMBER | FIGURE NUMBER | TRANSDUCER NUMBER | FIGURE NUMBER |
|----------------------|------------------|----------------------|------------------|----------------------|------------------|
| C4M | A-48. A-49 | D7A | A-60, A-62 | F4 | A-75 |
| C5M | A-50 | D8A | A-60, A-62 | F5 | A-9 |
| C6M | A-44, A-56 | D9A | A-60. A-62 | F6 | A-75 |
| C7M | A-51 | D10A | A-60, A-63 | F7 | A-76 |
| C8M | A-51, A-52 | D11A | A-50, A-64 | F8 | A-76 |
| C9M | A-53 | D12A | A-59, A-65 | F9 | A-8, A-77 |
| C10M | A-54 | D13A | A-60, A-64 | F10 | A-8, A-77 |
| C11M | A-45 | D14A | A-59, A-65 | F11 | A-78 |
| C12M | A-45 | D15A | A-60, A-64 | F12 | A-8, A-79 |
| C17A | A-55 | D16A | A-66 | F13 | A-22 |
| C18A | A-44, A-56 | E1M | A-31, A-67 | F14 | A-80 |
| C19A | A-44, A-50 | E2A | A-71, A-72 | F15 | A-8, A-81 |
| C2OA | A-44, A-57 | E3A | A-71, A-72 | F16 | A-81 |
| C21A | A-44 | E4A | A-71 | F17 | A-81 |
| C22A | A-44 | E5A | A-71 | FÍÉ | A-77 |
| C23A | A-45 | E6A | A-68 | F19 | A-74 |
| C24A | A-45 | E7M | A-39, A-69 | 1 13 | N=14 |
| C25A | A-46 | EllA | A-69 | | |
| C26A | A-4/. A-58 | E12A | A-69 | | |
| | | | | | |
| C27A | A-47, A-58 | E13A | A-70 | | |
| C28A | A-47 | E14A | A-71, A-73 | | |
| D1A | A-59, A-61 | E15A | A-71, A-73 | | |
| D2A | A-59, A-61 | A16A | | | |
| D3A | A-59, A-61 | A17A | A-71, A-74 | | |
| D4A | A-60, A-62 | F1 | A-22 | | |
| D5A | A-60, A-62 | F2 | A-10 | | |
| D6A | A-60, A-62 | F3 | A-8, A-26 | | |

Figure A-7 (Cont) Cross Reference: Transducer Number with Figure Number of Photograph Showing Precise Transducer Location

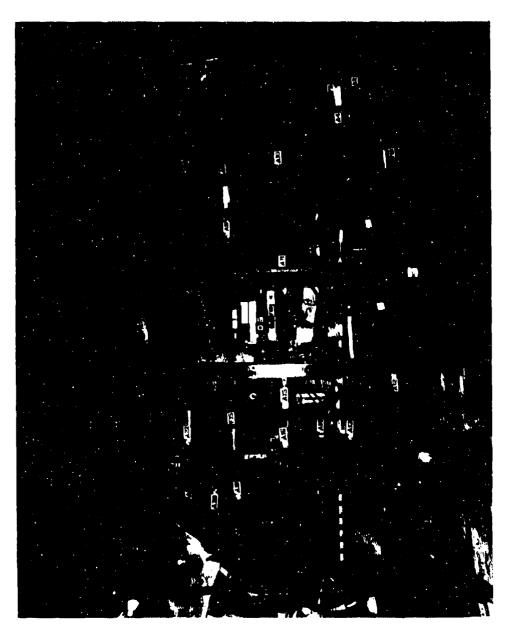


Figure A-8. Trandsucer Locations in Right Side Equipment Bay

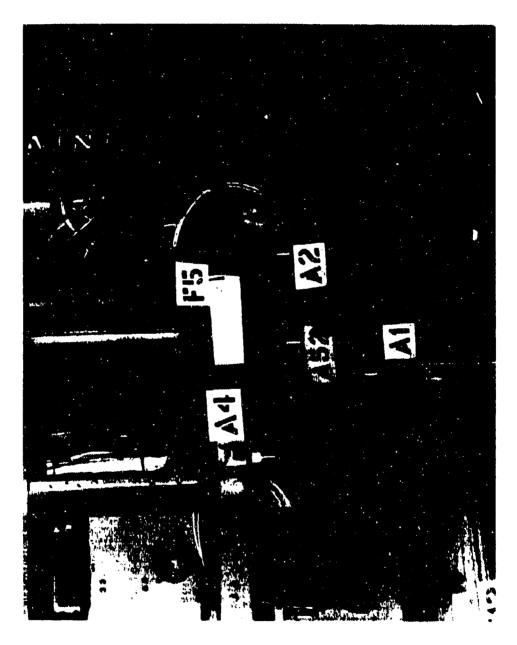


Figure A-9. Transducer Locations Near Ballistics Computer Compartment



Figure A-10. Transducer Locations Aft of TFR Computer Compartment

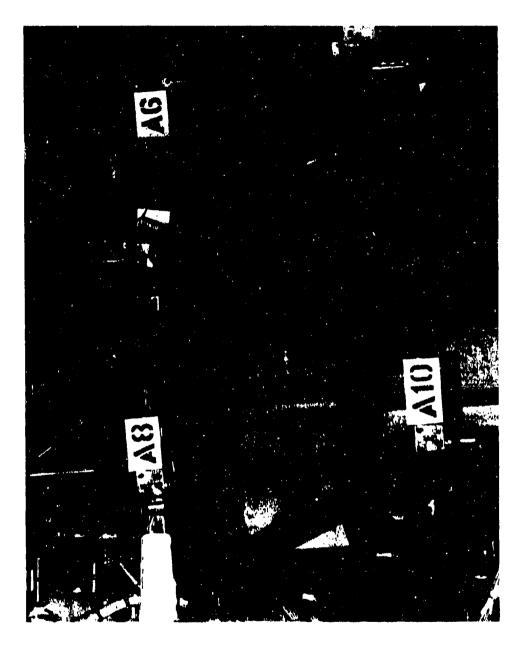


Figure A-11. Transducer Locations Near TFR Computer Compartment

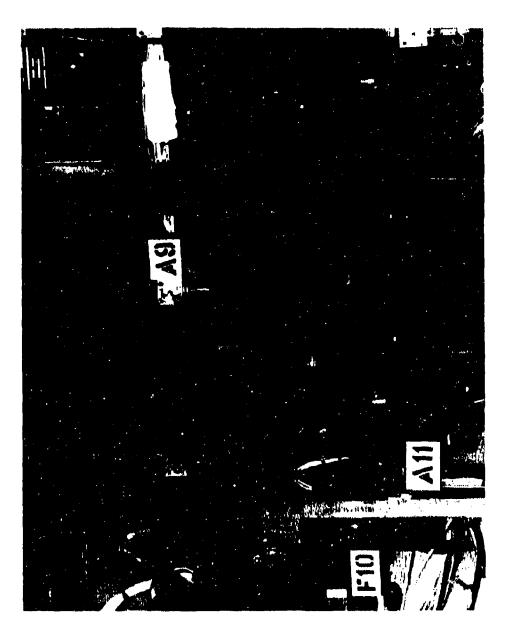


Figure A-12. Transducer Locations Near Power, AMP AN/ARC-112 Compartment



Figure A-13. Transducer Location Near ANT CONT AN/ARC-112

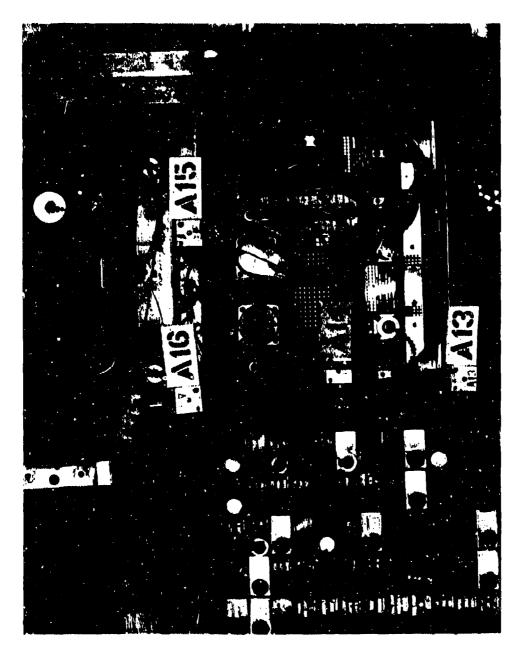


Figure A-14. Transducer Locations Near AN/ARN-52 Compartment

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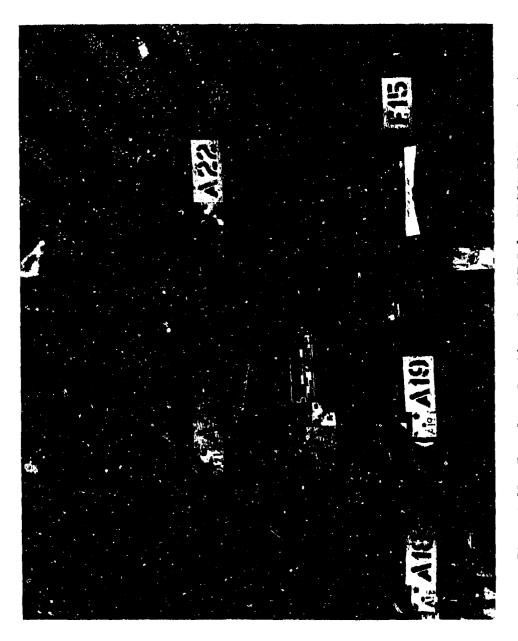


Figure A-15. Transducer Locations Near AMP Relay AN/ARA-50 Compartment

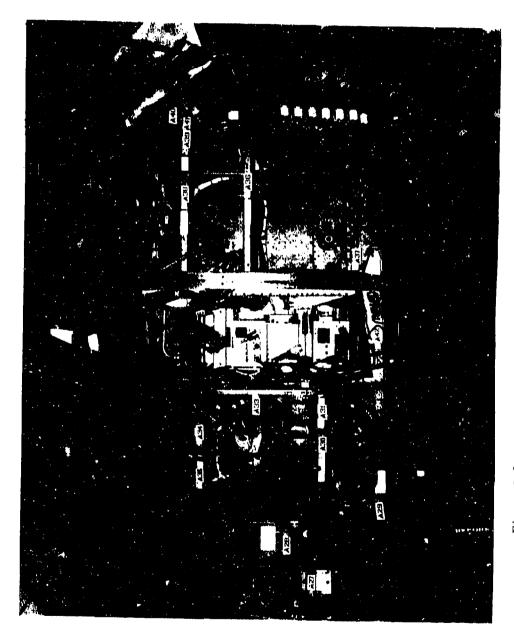


Figure A-16. Transducers Locations in Left Side Equipment Bay

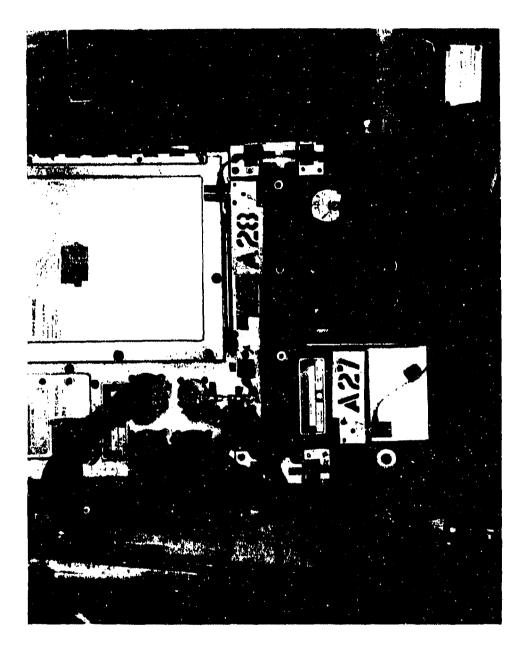
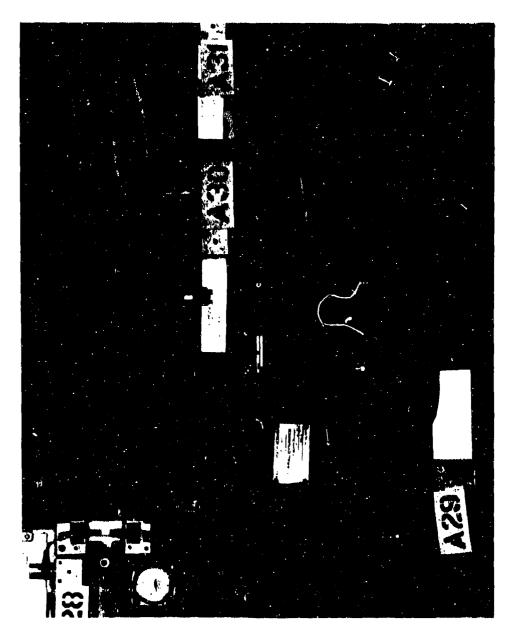
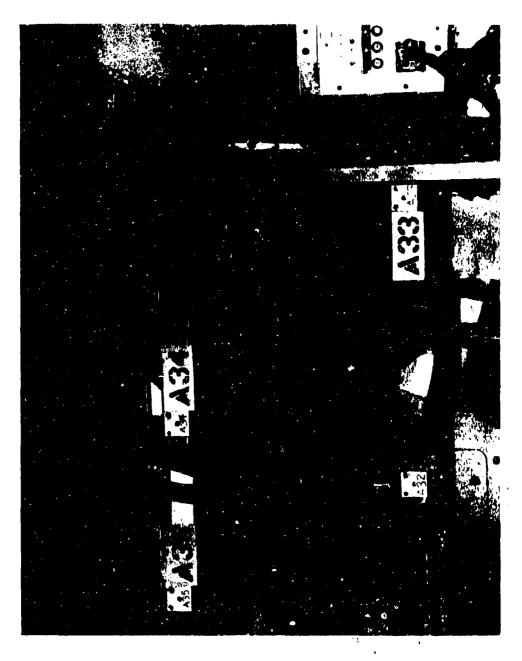


Figure A-17. Transducer Locations Near STACHRONIZER AN/APQ-113 Compartment



Transducer Locations Near Flight Control Computer Compartment Figure A-18.

国际经济运动的联节的基础的联节的联节的联节,



Transducer Locations Above Flight Control Computer Compartment Figure A-19.

- - 47

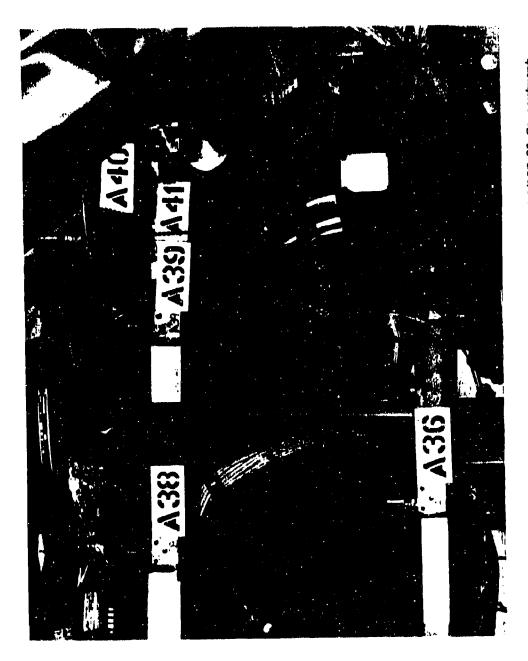


Figure A-20. Transducer Locations Near Computing Gyro AN/ASG-23 Compartment

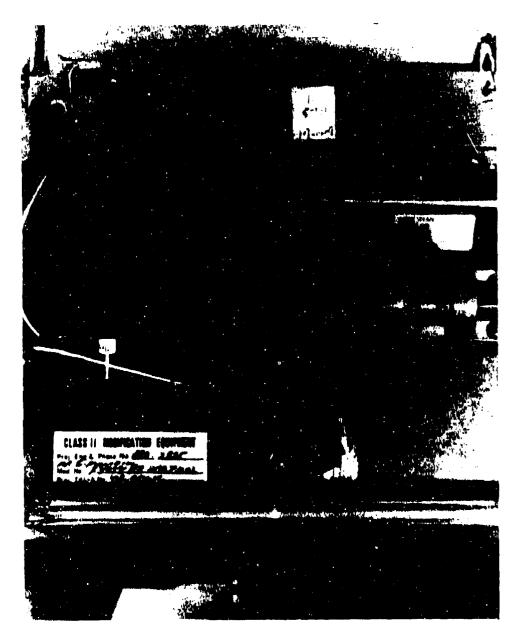


Figure A-21. Transducer Locations Near Amplifier AN/ALQ-94 Compartment

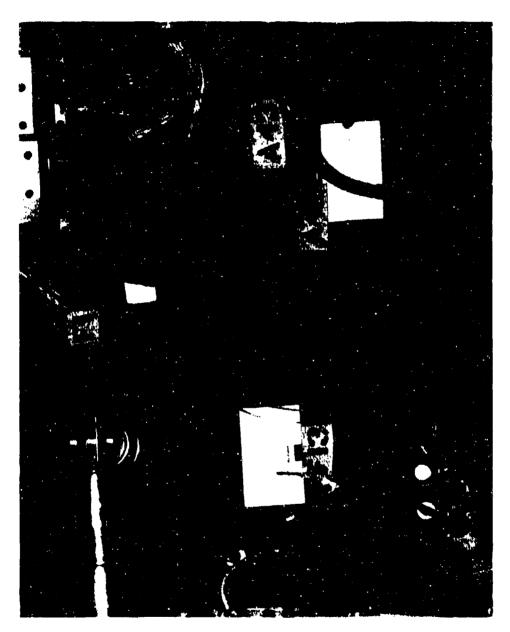


Figure A-22. Transducer Locations on Forward Side of Bulkhead Near Forward Looking Radar

Figure A-23. Transducer Location on Forward Bulkhead, Right Side Near Bottom Behind DC Power Panel



Transducer Location on Forward Bulkhead, Left Side Aft of Gen. Control Compartment



Transducer Locations on Forward Bulkhead on Left Side Aft of AC Power Transfer Assy Compartment Figure A-25.

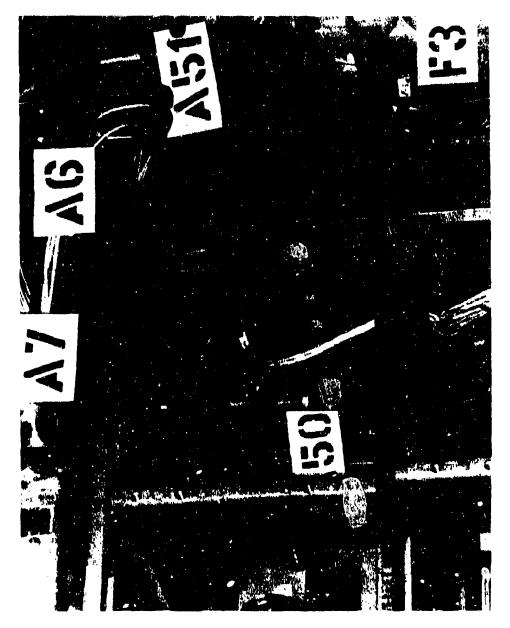


Figure A-26. Transducer Locations on Nose Bulkiead, Right Side Near Top of TFR Computer Compartment

Transducer Location on Right Side of Fuselage 65 inches Aft of Nose Tip in Radome Figure A-27.



Transducer Locations on Right Side of Fuselage 65 inches Aft of Nose Tip



Figure A-29. Transducer Locations on Underside of Fuselage at FS 145

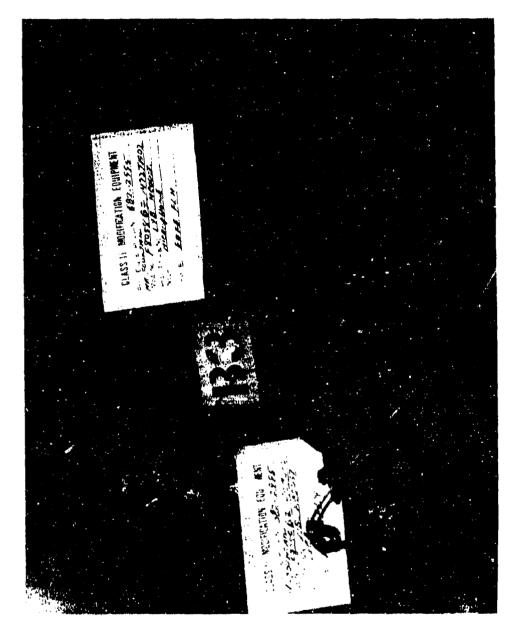
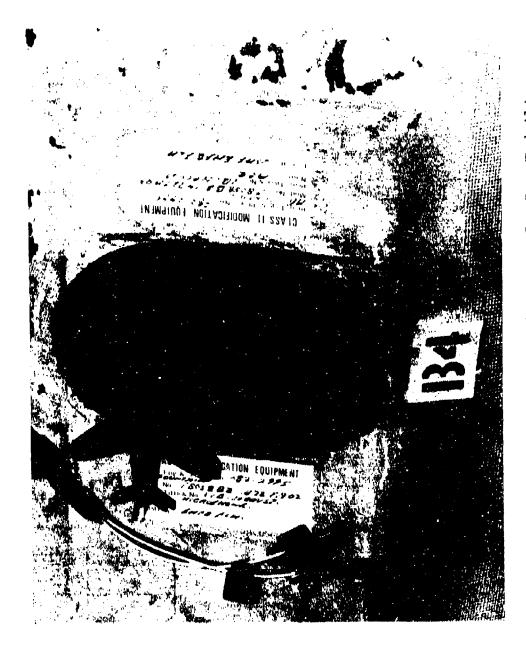


Figure A-30. Transducer Locations on Fuselage in Front of Oockpit at FS 155



Figure A-31. Transducer Locations on Nose Gear Door



gure A-32. Transducer Locations on Nose Gear Door (Backside)



Figure A-33. Transducer Locations on Right Side of Fuselage Below Canopy

Transducer Locations on Right Side of Fuselage Below Canopy Figure A-34.

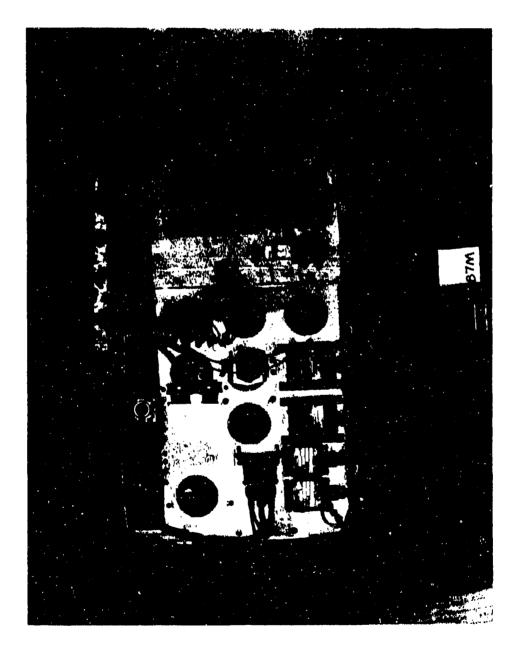


Figure A-35. Transducer Locations on Right Side of Fuselage At FS 357



Figure A-36. Transducer Locations on Top of Puselage Aft of Canopy at FS 370

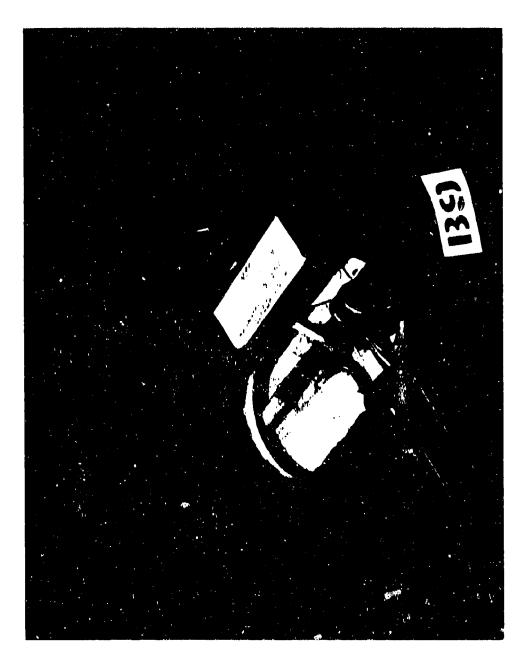


Figure A-37. Transducer Locations on Left Horizontal Stabilator

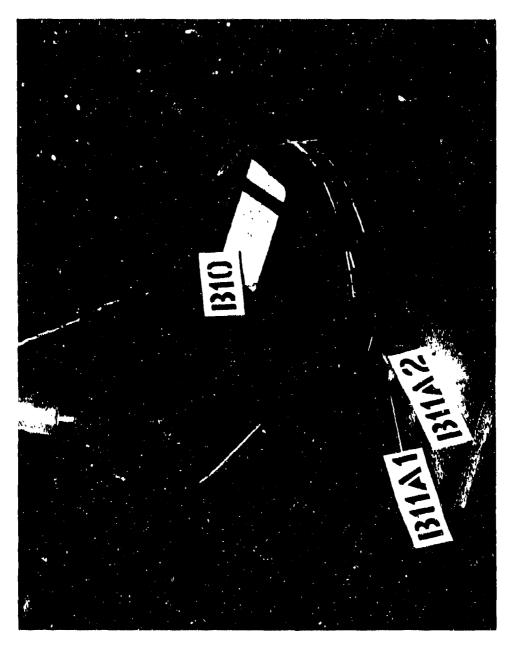


Figure A-38. Transducer Locations on Forward Left Side of Vertical Stabilator Near Fuselage

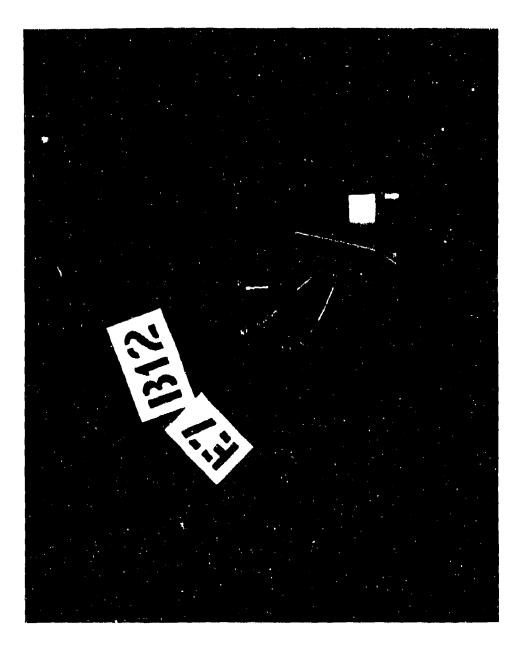


Figure A-39. Transcucer Locations on Top of Vertical Stabilator



Figure A-40. Transducer Locations on Left Inboard Wing

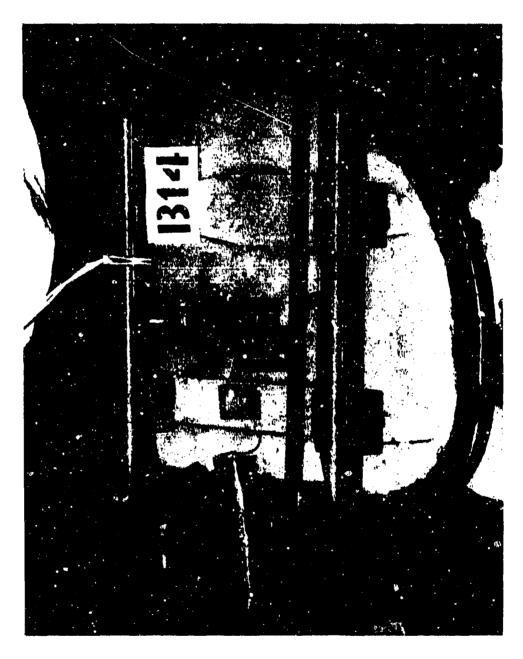


Figure A-41. Transducer Locations on Left Center Wing

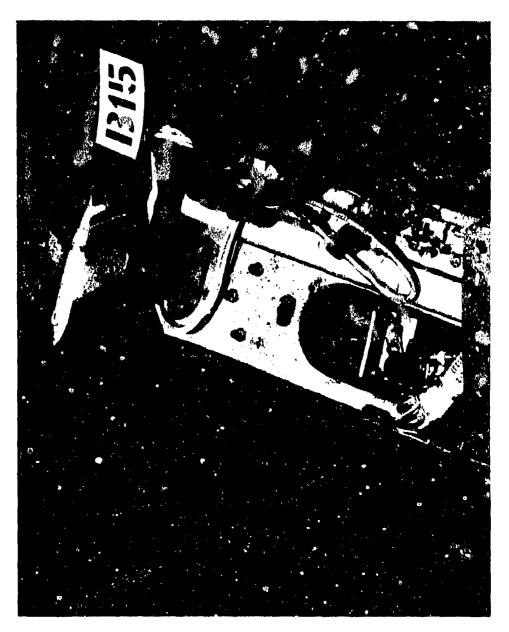


Figure 2-42. Transducer Locations on Late Cutboard Wing

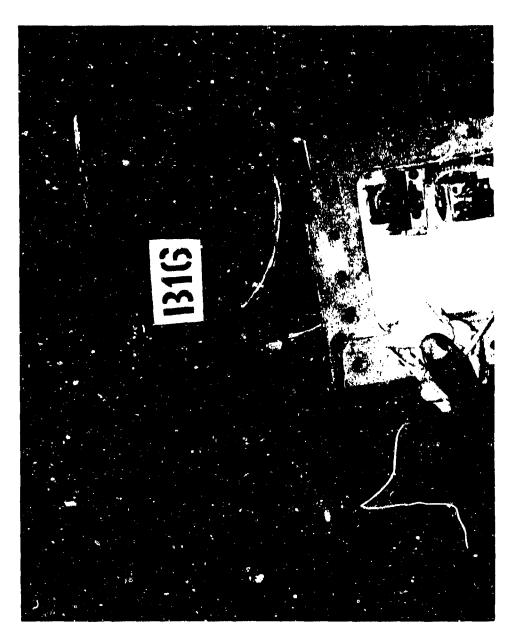


Figure A-43. Transducer Locations on Left Tip of Wing

A San Vigorial Bulgaria.



Figure A-44. Transducer Locations in Weapons Bay

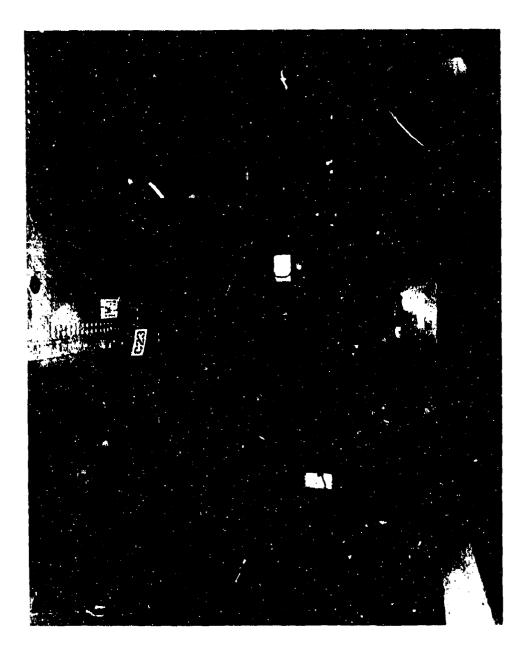


Figure A-45. Transducer Locations in Aft Section of Weapons Bay



Figure A-46. Transducer Locations on Upper Forward Wall of Weapons Bay

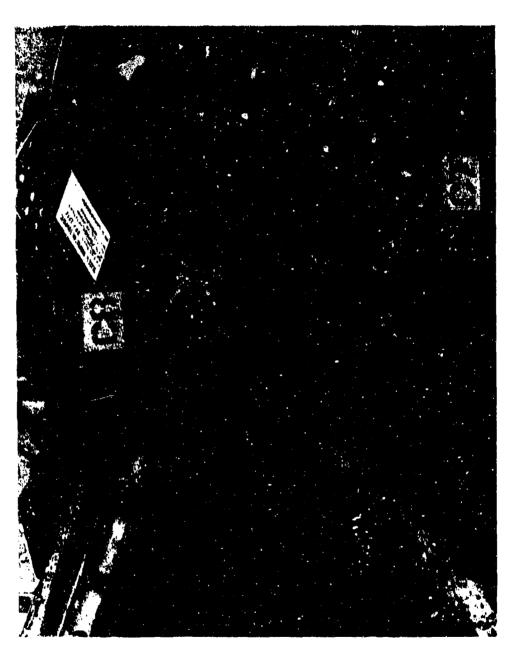


Figure A-47. Transducer Locations on Forward Wall of Weapons Bay

Figure A-48. Transducer Locations in Forward Upper Right Section of Weapons Bay

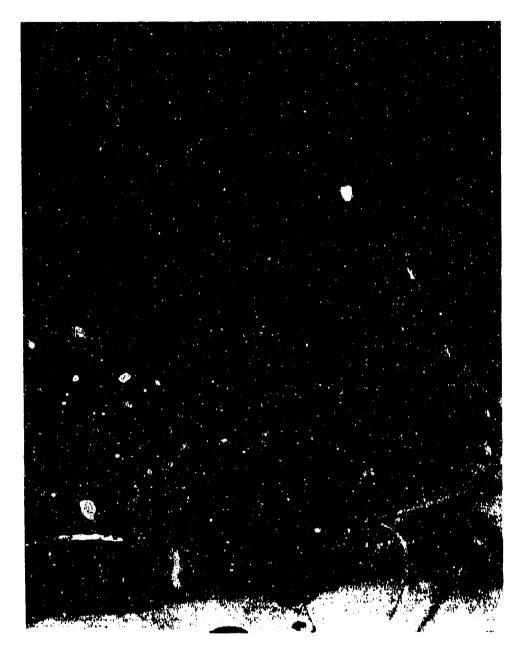
Figure A-49. Transducer Location in Forward Upper Right Section of Weapons Bay (Actual Location of C4M)

Transducer Locations in Forward Upper Left Section of Weapons Bay Figure A-50.

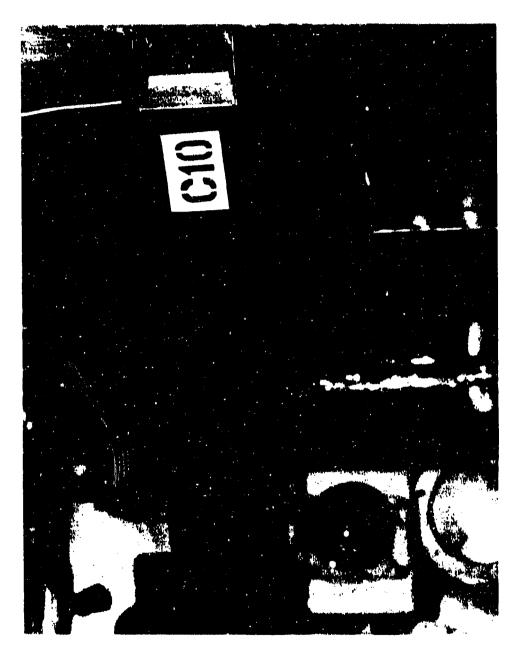


Transducer Locations in the Center Upper Right Section of Weapons Bay Figure A-51.

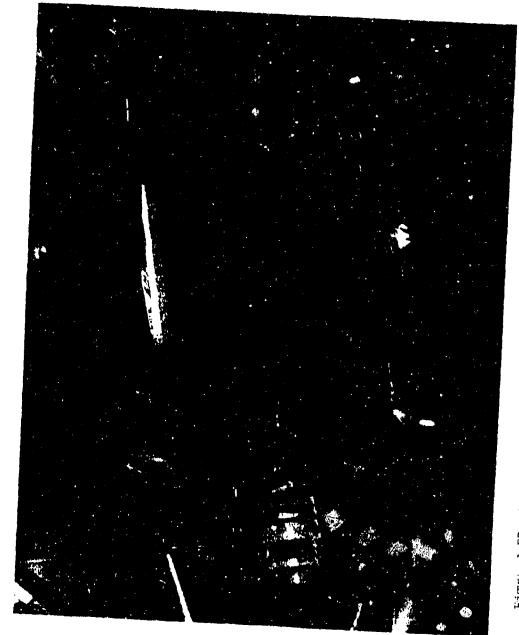
Figure A-52. Transducer Location in the Center Upper Right Section of Weapons Bay (Actual Location of CBM)



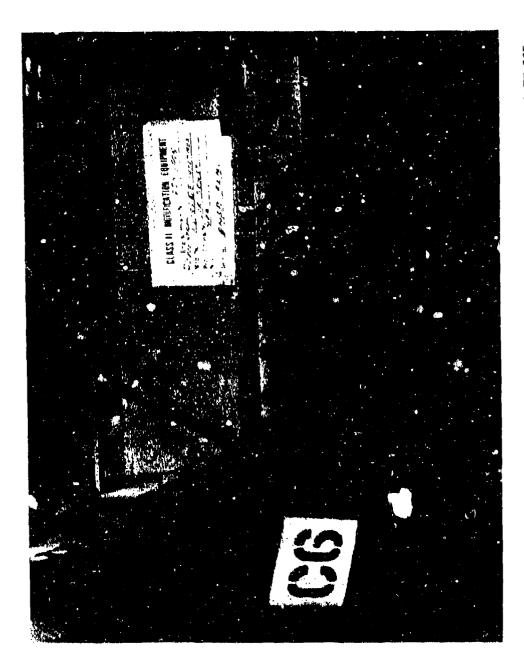
Transducer Locations in the Center Upper Left Section of Weapons Bay Figure A-53.



Transducer Location in the Center of the Left Wall of the Weapons Bay



Transducer Location c. Center Ceiling Beam of Weapons Bay at FS 280



Transducer Location on Center Ceiling Beam of Weapons Bay at FS 305 Figure A-56.

AND CLEARED FOR PUBLIC RELEASE.

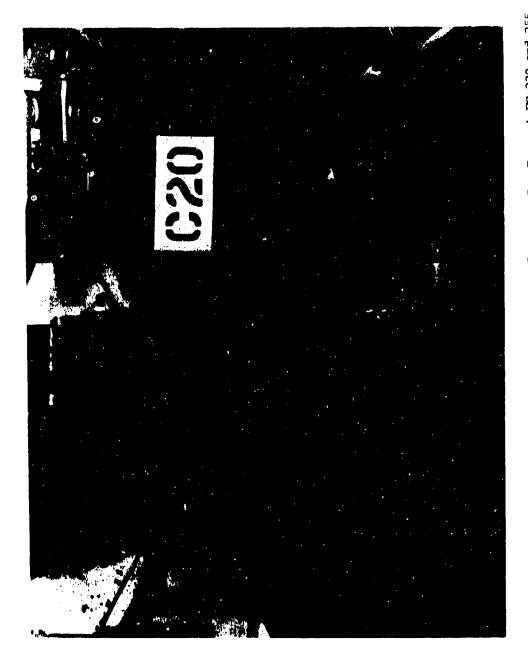
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**RESTRICTIONS ARE IMPOSED UPON

**TO USE AND DISCLOSURE.

MISTRIBUTION STATEMENT A

APPROVED FOR PUBLIC RELEASE;



Transducer Locations on Center Ceiling of Weapons Bay Beam at F3 330 and 355 Figure A-57.

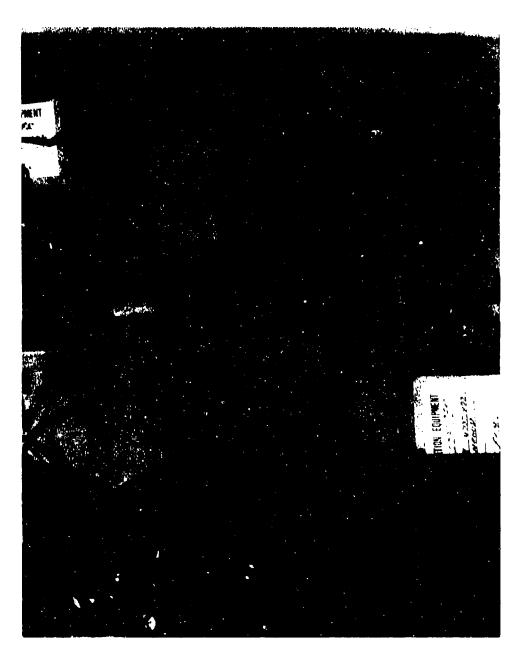


Figure A-58. Transducer Locations on Lower Right Center of Weapons Bay Forward Wall

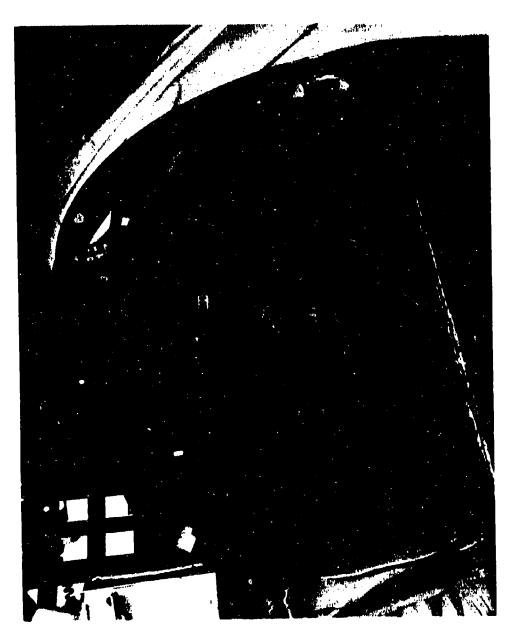


Figure A-59. Transducer Locations on Instrument Panel

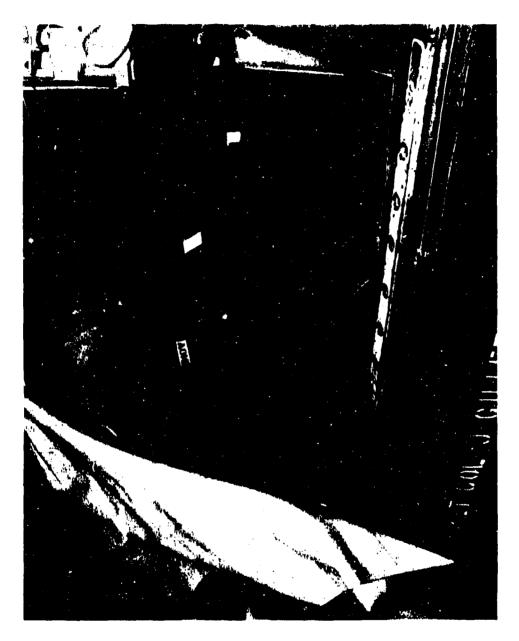


Figure A-60. Transducer Locations on Instrument Panel

Figure A-61. Transducer Locations on Left Sidewall near Bottom of Instrument Panel

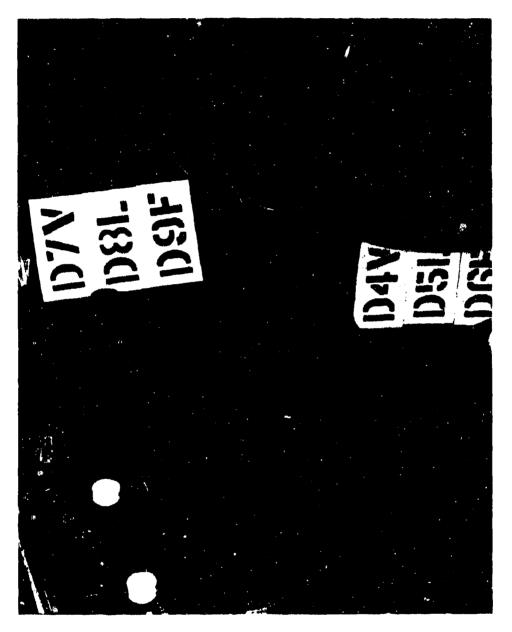


Figure A-62. Transducer Locations on Bottom Right Side on Instrument Panel and Sidewall

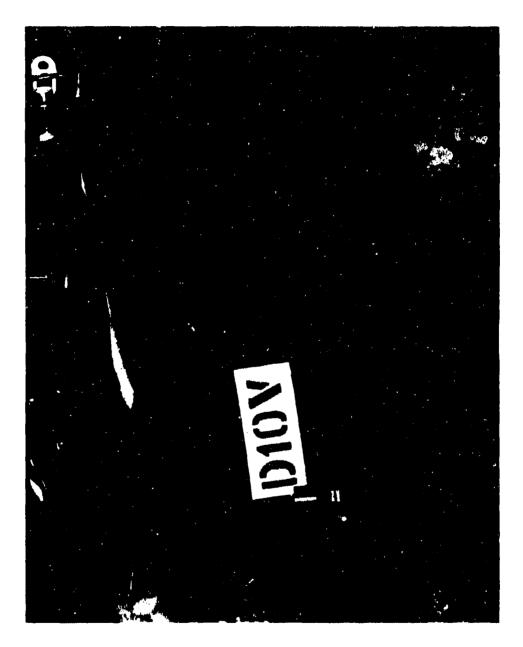


Figure A-63. Transducer Location Near Top of Instrument Panel Near Center

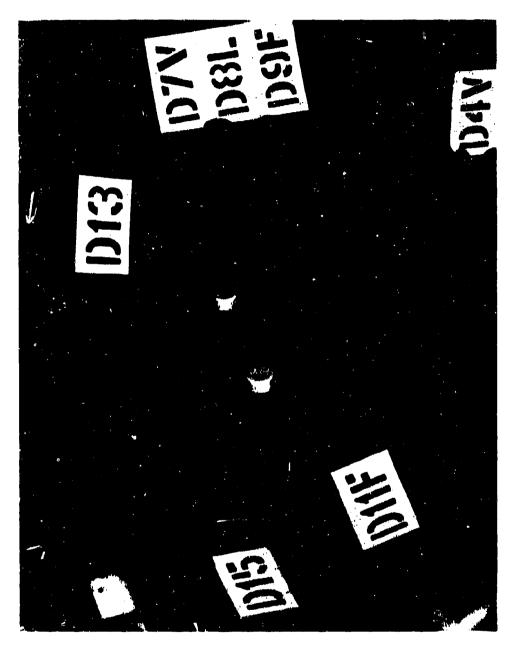


Figure A-64. Transducer Location on Right Side of Instrument Panel

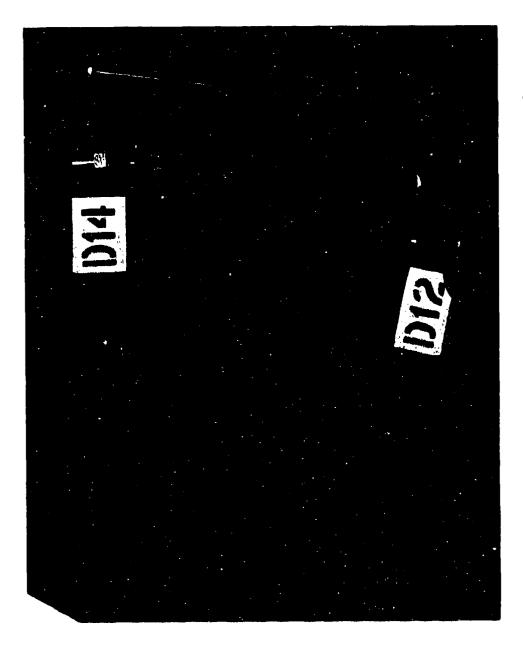


Figure A-65. Transducer Locations on Left Side of Instrument Panel



Figure A-66. Transducer Location on Center Console



Figure A-67. Transducer Location on Forward Landing Gear Door



Figure A-68. Transducer Location on Left Main Landing Gear Near Pivot

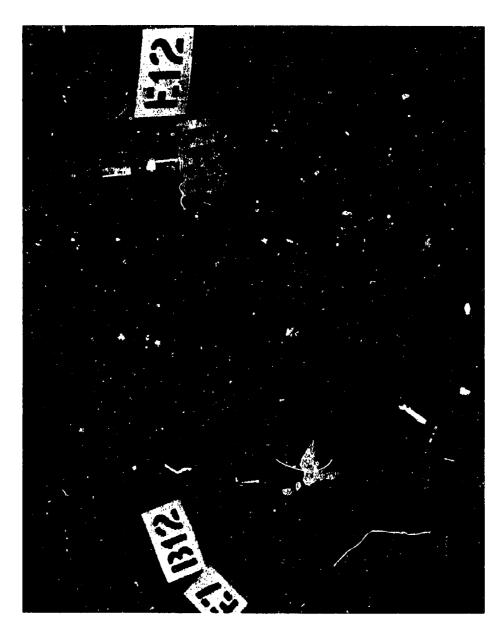


Figure A-69. Transducer Locations on Top of Vertical Stabilator

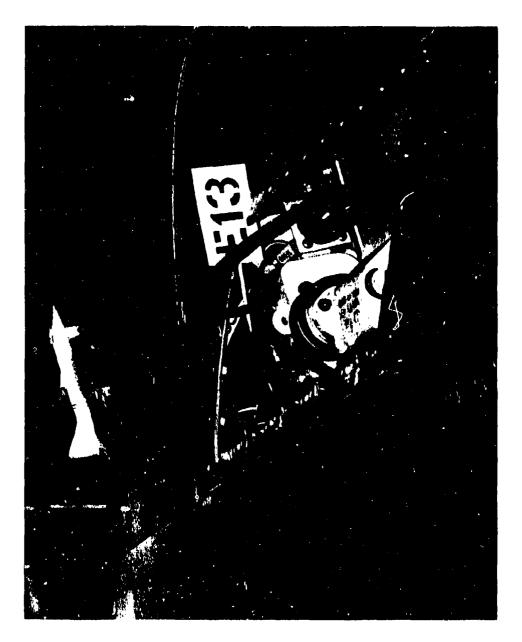


Figure A-70. Transducer Location near Tip of Left Wing

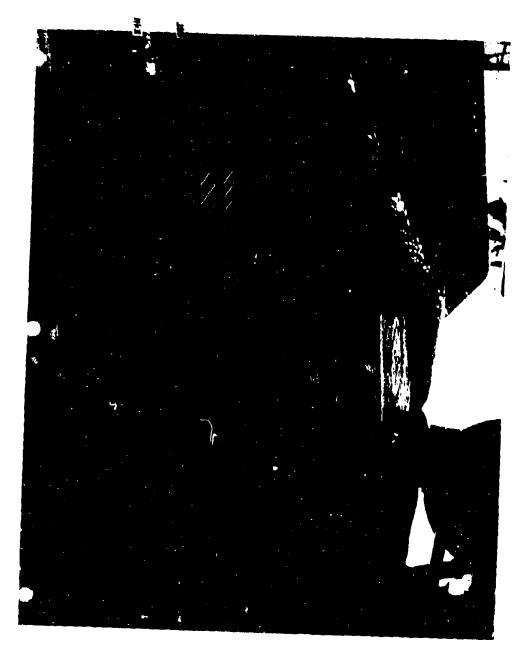


Figure A-71. Transducer Locations on Left Engine



Figure A-72. Transducer Locations on Left Engine Forward Mount

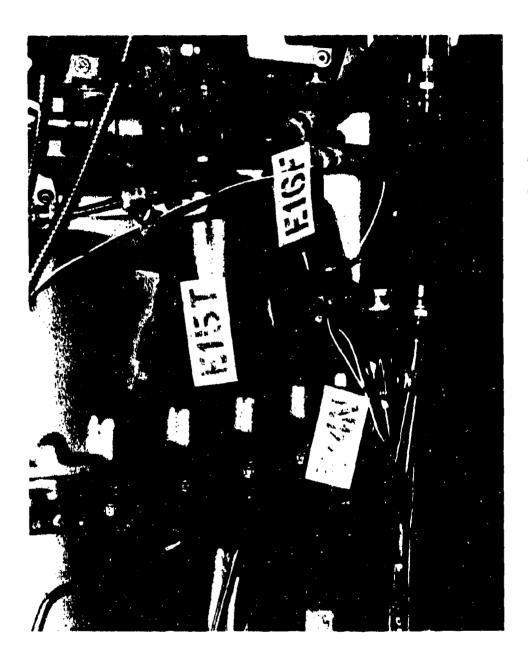


Figure A-73. Transducer Locations on Accessory Gear Box

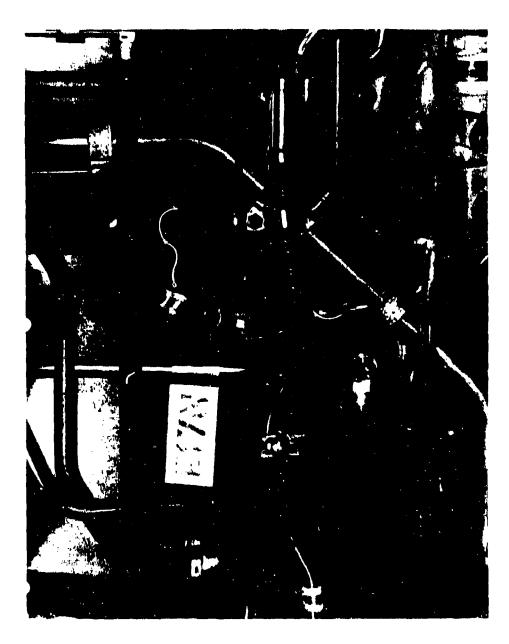


Figure A-74. Transducer Location on Firing Plug Terminal

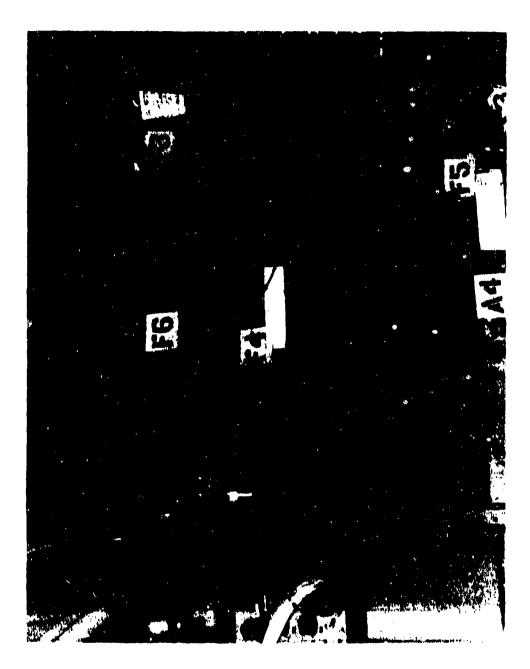


Figure A-75. Transducer Locations Near TFR Equipment Compartment



Figure A-76. Transducer Locations near TFR ECS Duct

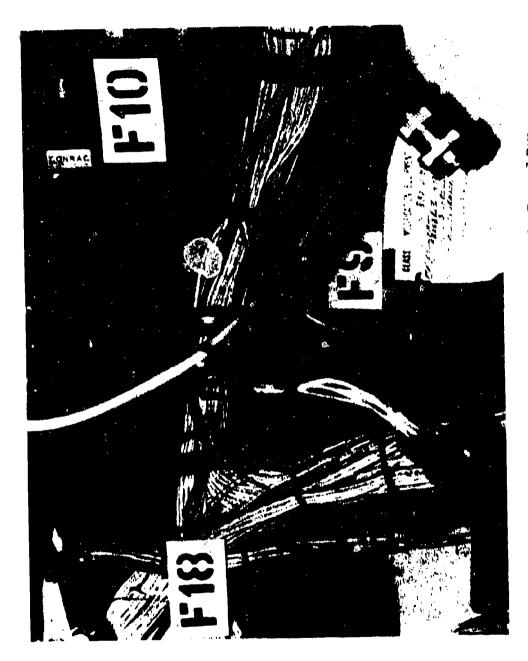


Figure A-77. Transducer Locations in Right Forward Bay



Figure A-78. Transducer Location on Right Forward Bay Door

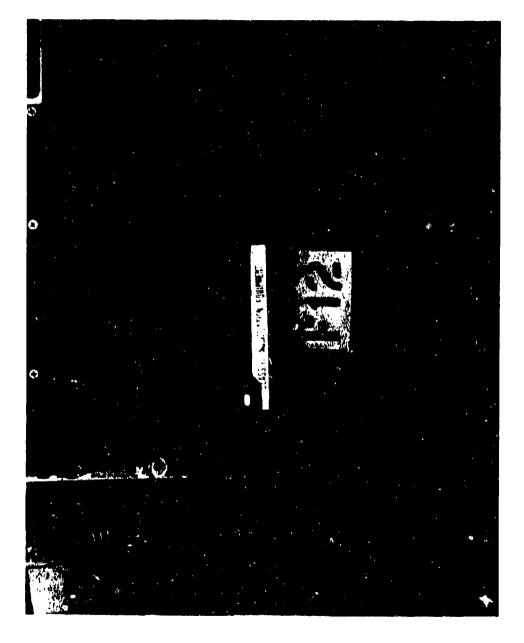


Figure A-79. Transducer Location Below Ballistics Computer Compartment on Structure

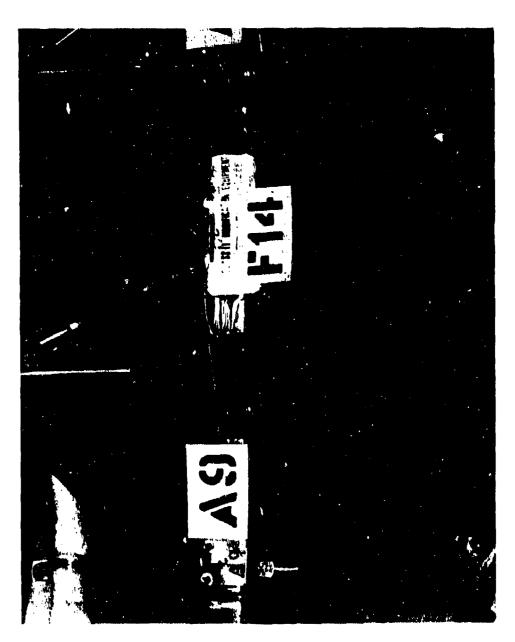


Figure A-80. Transducer Location Near Top of TFR Compartment



Figure A-81. Transducer Location Near AN/ARC-109 Compartment

TABLE A-1
DESCRIPTION OF TRANSDUCER LOCATIONS*

| the faces of the property of the first of th | |
|--|----------------------------|
| ALE VERT - ON STRUCTURE AFT OF BALLISTICS COMPUTER ASE WERT - PHO END OF HORIZ SUPPORT UNDER THE COMPUTER COMP. WEER SKIND. | 123 -26 147 |
| AJA LAV - 'ILAR AD | 120 -20 151 |
| AGA WORK - PUD INAIDE PLANCE WHERE BODY REETS CENTER OF YEAR CHAPT COMPANY COMPANY | 130 30 193 |
| ASA WORK - PHD INSIDE PLANCE MHERY DOOR MEETS CENTER OF THE CHPT COMPARTMENT ASA WERT - HOTIONTAL SUPPORT ABOVE THE COMPUTER COMP. NEAR BEHO | 119 -27 168 |
| ATA VERY - CENYER OF HEATE SUPPORT ABOVE THE COMPUTER COMP. | 129 -23 172 |
| ASA VERT - HOSE SUPPORT UNDER AFT CORNER OF RECEPTA RADAR APN-1AF | 137 -83 171 |
| | 146 -84 171 |
| ALGA VERY - PND CORNER OF HORIZ SUPPORT FOR POWER/AMP AW/ARE-118 ALIA VERY - AFT ENG OF HORIZ SUPPORT SPACKET FOR POWER/AMP AW/ARE-118 | 188 -24 161 |
| Atta year - PHD commen of support structure under ant cont anyanc-its | 174 988 144 |
| ALSA VERY - UNDER APT OUTER BHOCK HOUNT FOR COMPTR ASSY ALSA VERY - ON COMPTR ABBY ABOVE SHOCK HOUNT | 104 -24 154 |
| ALSA YERT - CENTER OF HORTZ BUPPORT UNDER ANJARC-189 | 177 -26 163 |
| ALOA WERT - ON HORES SUPPERT UNDER AFT CORNER OF ANCARC-LED | |
| ALGA VERT - AFT CORNER OF HORIZ SUPPORT ABOVE SEN CONTROL ALGA VERT - UNBER AFT DUTER SHOCK HOUNT FOR AMP RELAY ANYARA-ER | 202 -30 170 190 -30 170 |
| ANDA VERY - ON APP RELAY ANYARA-BE ABOVE SHOCK HOUNY | 198 -10 174 |
| ARIA VERT - AFT CORNER OF HORIZ SUPPORT FOR MATE AN/ARMATY | 198 +18 177 |
| AREA VERY - CENTER OF HOREE SUPPORY - FOR ENTR AN/ARN-FY ARE: YERT - UNDER FMD CORMER OF RYCHROMIZER AM/ARD-112 | 181 -38 177 183 18 149 |
| ARBA VERT - LOWER AFT CORNER REVRIXHTR MOB ANIAPO-113 | 135 13 183 |
| ARRA VERY - SUPPORY BUELF BY LOHER AFT HOUNT FOR SYNCHROMIZER | |
| ASSA VERT - CENTER OF MORTE SUPPORT UNDER FLIGHT CONT. COMPUTER ARIA VERT - AFT CORNER MORRE SUPPORT UNDER FLIGHT CONT. COMPUTER | 145 24 140 |
| A324 VERT - CENTER OF HORIZ SUPPORT JINDER FEEL & TRIM CONTROL | 144 24 189 |
| ASSA VERT - AFT CORNER OF HORIZ AUP BRACKET UNDER FEEL & TREM CONTROL | |
| A344 VERT - CENTER OF HORIZ SUPPORT UNDER AS/MACH AMP A354 VERY - PMD CORNER OF HORIZ SUPPORT UNDER ALT/YERT SPEED AMP | 147 23 144 |
| AS4A VERY - MORIE SUPPORT UNDER VID SIG PROCESS AN/APS-189 | |
| ASTA .VERT - PWD LOWER MOUNT BRACKET FOR STAB PLATFORM AN/AJS-26 | 178 18 144 |
| A384 VERY - UNDER AFT GUTER SHOCK HOUNT FOR COMPUTING AMP AM/ASE-23 A394 VERY - UNDER SHOCK HOUNT FOR COMPUTING SYRD AM/ASE-23 | 10B 3B 10P |
| A48A VERT - AFT CORMER OF HORTZ SUPPORT FOR STRO ANYASS-23 | |
| A41A FEA - CORNER OF HOMES SUP BRACKET FOR SYRD AN/ARRYED | |
| A424 VERT - STRUCTURE UNDER STABILIZED PLATFORM AN/AJG-88 AASA VERT - MEAR TOP RIGHT MOUNT OF FWD LOOKING RADAR FND SIDE OF ARMD | 178 27 14R |
| 444 FEA - NEAS 4434 | 114 40 184 |
| A48A NORM - ON SKHO HEAR BOTTOM BEHIND DE PONER PAREL | |
| A46A NORM - ON RKHO APT OF GEN, CONTROL UNIT A47A NORM - OM BKHO ART OF AG FORER TRANSFER ASSY COMP. | 707 24 168 277 22 154 |
| A48A NORM - ON REND BELOW A47 NEAR BOTTOM EDGE | 287 22 144 |
| AAPA NORY - ON HOSE MAND NEAR TOP REAR CONNER OF THE COMPUTER COMP. | 110 -10 100 |
| ASSA NORM - HEAR A49 ASSA NORM - ON HOSE SKHO HEAR TOP FRONT CORNER OF TER COMPUTER COMP. | 116 -16 167 |
| ABEA NORM - ON HOSE BEND NEAR SALLISTICS COMPUTER COMP. | |
| BIM PLUBH - CENTER OF RIGHT SIDE, 65" AFT NOSE TIP | 55 -24 178 |
| | 85 -80 170 |
| | 168 al 2 135 |

NOTE: Accelerometers are identified with an A and microphones with an M in the last character of the transducer ID. The transducers F1-F19 are thermocouples.

TABLE A-1 (Continued) DESCRIPTION OF TRANSDUCER LOCATIONS

| All throughout the form that the best and the party was true to the true and true | ے بت سیجے |
|--|--|
| 824 NORMAL TO SKIN HEAR BEH RIM PLUBH - NEAR TOP PHO OF CANOPY 12" LEFT OF C/L BIA NORMAL TO SKIN HEAR BIN | 145 -12 135 |
| MAN PLUPT A NEAR TOP, FIRST OF CANONY 18" LEFY OF EXL | |
| SJE NUTTAL TO DRIN NEAR BON SAM ON MON A AR PUR AN AREAN AND AND MARK APAR ASSA | 155 25 180 |
| BAM PLURH - 487 PMO OF MEATONS BAY ON HOSE GEAR DOOR | 230 7 136 230 7 136 |
| HAA NORMAL TO SKIN NEAR BAN HAN PLURM - \$13° AFT NORE SKHOL 21° RELGH BOTTOH EDGE OF RT CANCEY : 1 2103 | K30 / 13/9 |
| age under the first house which are the state of the stat | ************************************** |
| BOR MUNTHE TW CHAN REAN BON NAM WINDER TO GAR FAI | 263 -36 (76 |
| BSA NGRYAL TO SKIN NEAR BUM ASH FLUBH - F. J. 288 C/L 364 NGRWAL TO SKIN NEAR BOM | 842 -38 176 |
| BEA HORMAL TO SKIN HEAR BEN ATH FLUEN - CENTER OF PANEL 2286 RJ SIDE | - 10 ion |
| BYA NORMAL TO SKIN NEAR BYM | 357 -30 140 |
| BYA NORMAL TO SEEN NEAR BYM RBM FLUBM - ON FANEL RABR, 4° APY OF FWD EDBE RBA NORMAL VO BEEN NEAR BBM | 764 78 126 |
| BEA NORMAL YO SKIN NEAR BEM | 374 30 120 |
| HOM FLUEN - PANEL UPPER ACCESS TO TORONG TUREZHORIZ SIAB LEFT SIRE | |
| | |
| BIBH FLUSH - YERT' STAB' FND LEFT PANEL NEAR PUSELAGE | 718 |
| BIBA NORMAL TO BKIN NEAR BIBM | 710 5 210 |
| BIBS NORMAL TO SKIN NEAR SIGH BIAN FIR - NEAR BIR BIAN PERT - NEAR BIR | 707 1 910 |
| Bilds VERT - NEAR BIS | 707 6 216 |
| ALAM PLUEM = TOP OF VERTICAL STABILIZES | |
| BIZA NORMAL TO SKIN NEAR BIRM | 676 6 316 |
| BISM FLURH - INSOARD LEFT HIMB | |
| BIJA HORMAL TO SKIN HEAR BIJM | \$19 18F 288 |
| GIZA NORMAL TO SKIN NEAR BIZH AISM FLURM - INGOAD LEFT WINS GIZA NORMAL TO SKIN NEAR BIZH BIZH FLURM - CENTER RET WING GIZA NORMAL TO SKIN NEAR BIZH BIZH FLURM - QUIZH NEAR BIZH BIZH NORMAL TO SKIN NEAR BIZH BIZH NORMAL TO SKIN NEAR BIZH | ومقيب تنسفيني |
| BIAA HORMAL TO SKIN NEAR BIAM | 200 100 800 |
| BISH PLUSH - OUTBOARD LEFT HING. | |
| BISA NORMAL TO SKIN HEAR BISH BISH PLUSH - TIP OF LEFT NINS | BA9 290 200 |
| BIGA NORMAL TO SKIN NEAR BIGM | 110 20% |
| TIGA NORMAL TO SKIN NEAR BIGM CIM FLUBM - MEAPONS BAY FWD WALL DNE-FORTH DOWN RIGHT BID? CEM FLUBM - MEAPONS BAY FWD WALL MIDNAY DOWN LEFT BIDE | 658 318 298 278 -12 143 |
| CAN PLUSH - MEAPONS SAY PHO WALL MEDWAY DOWN LEFT SIDE | - 278 -12 143 278 11 147 |
| CON PLUSH - WEAPONS BAY SE" AFT FOR HALL HIGHE DE RIGHT MALL | _ <u> </u> |
| CIM FLUSH - MEAFONS BAY FMD MALL MIDWAY DOWN LEFT SIDE CAM FLUSH - MEAFONS BAY SI AFT FOM MALL MIDDLE OF RIGHT MALL CAM FLUSH - MEAFONS BAY SI AFT FMD MALL, RIGHT SIDE OF CEILING COM FLUSH - MEAFONS BAY SI AFT FMD MALL, LEFT SIDE OF CEILING COM FLUSH - MEAFONS BAY SI AFT FMD MALL, MIDDLE OF REFT WALL COM FLUSH - MEAFONS BAY 128" AFT OF FMD MALL, MIDDLE OF REFT WALL COM FLUSH - MEAFONS BAY 128" AFT OF FMD MALL, RT. SIDE OF CEILING COM FLUSH - MEAFONS BAY 128" AFT OF FMD MALL, LEFT SIDE OF CEILING COM FLUSH - MEAFONS BAY 128" AFT OF FMD MALL, HIDDLE OF LEFT WALL GIM FLUSH - MEAFONS BAY 128" AFT OF FMD MALL, HIDDLE OF LEFT WALL COM FLUSH - MEAFONS BAY AFT MALL ONCECORTA DOWN RIGHT CENTER | 320 47 147 |
| COM PLUSH - WEAPONS BAY SIR AFT PWD WALL, LEFT SIDE OF CETLING | 320 8 147 |
| CAM FLUSH & MEAPONS BAY 51" AFT PHD HALL, MIDDLE OF EFT WALL | 390 28 143 |
| CTM PLUSH - WEAPONS BAY 128" AFT OF FHO WALL, MIDDLE OF RIGHT WALL | 398 -28 197 |
| CON FLUEN - HEAPONS BAY 128" AFT OF PHO WALL, RY, SIDE OF CEILING | 396 -21 173 |
| CRM FLURM - MEAPONS BAY 1285 AFT OF FHO MALL LEFT SIDE OF SELENG | |
| CIBH FLUBH - MEAPONS BAY 128" APT OF PHD HALL, HIDDLE OF LEFT HALL | 398 28 187 |
| GILH FLUGH - HEAPONS BAY AET MALL ONE-EDRIH DOWN RIGHT GENTER | |
| | 466 15 165 |
| CIPA VENTA - CENTER CEILING BEAM OF MEAPONS BAY AT FR 28P | |
| clas Acute a regime referan actual of actions and by the 24s. | 700 18 166 |
| CIDA VERTA - CENTER CELLING BEAM OF PEAPONS BAY AT PA 338 | |
| CZBA VERT, - CENTER CELLING BEAM OF MEAPONS BAY AT PS 358 CZIA VERT, - CENTER CELLING BEAM OF MEAPONS BAY AT PS 388 | 305 0 171 |
| C224 VERT CENTER CELLING BEAM OF MEAPONS BAY AT F8 488 | |
| C22A VERT, - CENTER CEILING BEAM OF WEAPONS BAY AT F8 488 C23A VERT, - CENTER CEILING BEAM OF MEAPONS BAY AT F8 488 C24A VERT, - CENTER CEILING BEAM OF MEAPONS BAY AT F8 488 C26A VERT, - CENTER CEILING BEAM OF MEAPONS BAY AT F8 488 C26A VERT, - CENTER CEILING BEAM OF MEAPONS BAY AT F8 488 C26A VERT, - CENTER CEILING BEAM OF MEAPONS BAY C26A VERT, - CENTER OF FMD MAIL OF MEAPONS BAY | 424 4 174 |
| CARA VENTA - CENTER CEILING BEAM OF MEAPONS BAY AT FS 455 | |
| CANA YORK A UPPER RIGHT CENTER OF THO HALL OF HEAPONS BAY | EAT THE TEN |
| CASA YORY - MICHT CENTER OF FHD HALL, OF HEAPONS BAY | 277 -12 198 |
| COTA YORM - LOHEN RIGHT CENTER OF FED HALL OF HEAPONS BAY | 27 -12 143 |
| CZSA NORM - LEFY CENTER OF FURNARD - ALL OF HEAPONS BAY | 7 4 6 110 |
| C28A HORN - MIDHT CENTER OF FHD WALL, OF HEAPONS BAY C27A HORN - LOYER RIGHT CENTER OF FFD WALL OF MEAPONS BAY C28A HORN - LEFF CENTER OF FORWARD - ALL OF MEAPONS BAY O1A VERT - STOEWALL BELOW LY' BOTTOM CORNER OF INSTRUMENT PANEL | 212 24 174 |

TABLE A-1 (Concluded)

DESCRIPTION OF TRANSDUCER LOCATIONS

| DZA LAY - NCAR DIA | 137 | - 24 | 176 |
|--|------------------|------------|----------|
| DJA FAA - NEAR DIA | | 24_ | _121. |
| DIA VERT - SIDEWALL BELOW RY, BOTTOM CORNER OF ENSTRUMENT PAREL | 231 | -27 | 173 |
| PPA LAT - NEAB DAA | | <u> </u> | Ή |
| DEA PLA - HEAR DAA | 131 | -87 | 173 |
| DZA WERT - ON INSTRUMENT PANEL LOWER RIGHT SIDE | - 131 | <u></u> | izi |
| DOA LAY - NEAR DYA | | -24 | 176 |
| DIGA VERY - NEAR TOP CENTER OF INSTRUMENT PANEL | 200 | | 101 |
| OLA PLA - 5" OFF CAL LOWER INSTRUMENT PANEL DN TAGAN ARN-84 MNIT | 156 | _ = = 1 | iii |
| DIZA VERY - CENTER OF LEFT INSTRUMENT PANEL | - 250 | 11 | 107 |
| OLSE WEST - CENTER OF BIGHT WATERWENT CANEL | _231_ | _نند_ | |
| DI4A VERT - ON RIGHT SIDE HOUNT OF GUN STORT | 228 | 37 | |
| DÍRA VERT - NEAR DÍIA " | * 230 | | iää |
| DIGA VERT - AFT ON CENT CONSOLE ON ARC-1990, C-6364, CONTROL RECEIVER TRANS UNIT | -187 | -4 | 737 |
| PIM PLUSH - PWD LAMDING GEAR DORM, MIDDLE, 18" FHD OF AFT EDGE | _241_ | | 121 |
| CZA HORMAL - LEPT ENGINE LT PHD HOUNT | (3) | 68 | 170 |
| ESA TANGENTIAL - LEFT ENGINE LT PHO HOUNT | 130_ | | 120 |
| C4A NORMAL - LEFT ENGING LT AFT MOUNT | 400 | | 1 48 |
| EBA TANGENTIAL - LEFT ENGINE LY AFT MOUNT | | | 144 |
| ESA VERT - LT MAIN LANDING SEAR UPPER HEAR PIVOT (FOR LANDING LOADS) | - 562 | 10 | 148 |
| CZM PLVAN - GENTER OF VERT STAB 1" BELON RISM | <u> </u> | | -žië |
| ELLA VERT - TIP AFT OF VERY SYAB ON STRUCTURE | 176 | 518 | |
| CISA VERT - PHO TIP OF LEFT WING | - 178 | -318- | ₩ |
| TIMA NORMAL - ON ACCEBBORY OF AR BOX | 140 | | 145 |
| CIBA TANGENTIAL - ON ACCEBBORY GEAR BUX | 440 | | 145 |
| FIGA FRA TON ACCESSORY BEAR ROK | 648 | _ ## | 140 |
| EITA TANGENTIAL - ON PIRING PLUS TERRINAL, LEFT ENGINE | 848 | 40 | 140 |
| PI TYCE - SURFACE TEMP PHO STOR OF BULNAFAD INSTOR RADOME | | 7 | |
| E Allegado Deus' 100 Asar Ad Mare Alli Plina | | -24 | 166 |
| The TACH - ARE TEMPS NEAR AFT STOP OF HOSE BULKHEAD | | ŽŠ | JAA. |
| L4 1204 a noife: see Win isule its issuchties | 129 | -29 | 101 |
| PR Y/CO - SURFACE TEMPA TER ' E SUFFERT (FMP) | 122_ | | _153_ |
| F6 T/C6 - TFR TRANSMITTER OUTLET CCS AIR TEMP. | 1 # 6 | -10 | 143 |
| FY T/CF - IFB CGR ATR INLET TEMP, CIN DUCT) | | سللعب | |
| FR AFR - TER ECG AIR FLOW RATE (IN DUCT) | 141 | -14 | |
| PO HUM - TPM ECS AIR INLET DEMPOINT TEMP. (IN DUCT) FI & PRES H RIGHT FORMARD BAY PRESSURE | 141 _ | F.I | |
| FI & TYCE - RIGHT FORMARD BAY DOOR SKIN SURFACE TEMP. | 147 | -24 -26 | 163 |
| DI A - JPA - BUAPIAR DEMA RE ESTIAN STRUCKS BY STAND STAND | 4 | -21 | 122 |
| PI 3 TERE - ATT TEMP, PND SIDE OF BULKHEAD INBIDE MADDE | 114 | | |
| PI 4 T/CLE - AIR TEMP. ABOVE AND LEFT OF TER | 134 | | 171 |
| TI B TZC12 - AIR TEMP. ABOVE ARC-104 | iñi | 30_ | 170 |
| PI 6 YCCIS - AIR YEMP, AFY OF ARC-164 | 113 | -26 | 147 |
| FI 7 T/C14 - OUTLET AIR FCR TEMPA OF ARC-104 | …išā. | | _i i i . |
| PI B APR - ECG AIRFLON RATE TO ANYARE-189 (IN DUCT) | 170 | -14 | 102 |
| PI O TECES - EPT ENGINE NEAR EST | | 69_ | 141 |

TABLE A-2

PUID/CHANNEL/SWITCH POSITION MATRIX

| | œ | |
|-------------|------------|---|
| | 1 | FEGA FILVA FILVA FILVA CLIIM C |
| | 134 | A3A A33A A133A A133A E113 C181A C22A D9A |
| | 128 | A424 A944 A144 A164 E124 C124 C127 C127 E64 E134 E134 |
| | 124 | A28A A7A A15A A15A C9H C9H A48A E71 |
| | 10 | A 52A A 53A A 53A A 26A D 12A D 12A B 15A C 7 M C 7 M |
| | 6 | A27A A6A A14A A14A A14A E2A B16A B16A C21A C21A A52A A52A A52A |
| | • | A11A A11A B19A C15H C15H C15H C15H C15H C15H C15H C15H |
| | ^ | AUSA BUSA BUSA CCSA CCSA CCSA CCSA CCSA CCSA CCSA C |
| | • | A29A A49A B2A A33A B5H B7A B13A C24A C27A C27A |
| | 1 0 | AUGA BUSA BUSA BUSA BUSA BUSA BUSA BUSA BUS |
| APE CHANNEL | M | A22A A22A A12A B6A B14H C12A A23A C13A |
| TAPE C | ~ | A14 A214 A214 A114 A114 B3A B3A B3A C14 C17 C254 C254 |
| | | - 0 50 4 50 60 60 FE |
| | | 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 |

(VOICE-CH#1 PCM-CH#4811 TIME-CH#14)

TABLE A-3 Athoraft test configurations

| Switch Position Gam Fire | | | | | | | | | | | | | | | | | | | | | | | | | • | 1,2,3,4,5 | 1,2,0,7,8,3 | 10,11,17,1,6,5 | 5.9.10.11.12 | | | 1,2,3,4,5 | 1,2,3,4,5 | | | | | |
|---|----------|-------|-------|-------|-------|-----------|---|-----------|----------|---------------------------------------|-----------|-------|-------|-----|------------|----------------|-------|---------------|-----|--|--------------|-------|-----------|----------|-----------------|-----------|-------------|----------------|-----------------|----------|----------------|-----------|-----------------|--------|----------------|------------|-------|-------|
| Sta6 | Pond | 3 | | | | į | \ 20 20 20 20 20 20 20 20 20 20 20 20 20 | ě | | 8 | ğ | Š | | ĺ | į | ž, | | į | | 12 12 13 13 13 13 13 13 13 13 13 13 13 13 13 | | | Š | 20 | | Ĭ | | | Ā | 1 | 7 | X X | 3 | S | | į | 202 | |
| ration Stas. | Hone | 2 | 8 | 1 | | į | 100 | 3 | ۶ کار | ě, | | | j | 505 | 5 | | Į, | ě | | 7 | | | 1 | | ě, | | | | 3 | 3 | 75 | ¥ | 3 | | | | 200 | 3 |
| External Store Configuration Stal, Staf, Staf, | Kone | 8 | Pope | \$ | | ŝ | 1007 | 3 | 100, | | | | 3 | | | - 100 E | | | | CT0-2 | | Fore | Mone | e de | | | | | ¥84 | MOR | 7-25 13-7-3 | ı | #K34 | 1 | | a de | Pore | 200 |
| Store (Sta3, | Bone | Hone | 200 | Hone | | 3 | 100/8 | Kone | į | | | | 5 | | eg . | | | 2 | Ę | 2-AL-2 | i | 2 | Ž | | | | 8 | , S | ij | B | 7 | ¥ | Ž | 1 | 1 | ğ | 2 | 3 |
| Spoiler Configu- ration #1, #2, #3 | Clem | Clean | Clean | | Cless | Clean | | Clean | 7.00 | | #2 C# | 2 | := | ; | 4 : | 7.4 | 12 | | : | 1 | 1# | 1 | = | : | : | - | * | Mone | None | None | None | #GJe | Kone | - Bone | 20 | 1 | 15 | 45 |
| Switch Posi- tion for Weapons Bay Doors Open | 1,9,9 | Kore | Kone | m | • | 6.0 | | Øn. | • |) 0 | | TORE. | 8,9,8 | | D. 00 C | ا ان ان | 0 0 | 7 6 6 | | Fore | Nose | • | 8,0,0 | | - | · • | | 8,9,8 | None | 8,9,9,8 | Pone | | Pore | 87.6 | e0 | 80 | 8,9,8 | 200 |
| Right Weapons Bay Configu- ration | Clein | Clean | Clean | Clean | Clean | Clean | | Clean | 1 | | | Clean | 8-noa | | 8-70H-8 | 2-1-8 2-1-8 | 200 | Gun (No Amen) | | Gun (Ho Ameo) | Gun (No Ame) | 3 | - | | Gun (27 Brands) | X | × | ğ | Gen (2X Rounds) | Ø | _ | <u>K</u> | Gun (2K Rounds) | Clean | 8-00g | Clean | Clean | Clean |
| Left Weapons Bay Configu- ration | Clean | Clean | Clean | Clean | Clean | Clean | | Clean | 200 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 1 to 1 | Clean | 800-8 | į | | 200 S | Clean | | | Clean | Clean | Clean | 9-703 | | | Clear | Clean | Clean | Clear | 8-ng | Clear | | CIERO | Clean | 800-8 8-003 | | | Clean |
| Flight Date | 5 Oct 79 | Ş | Ş | ä | ě | Ą | | 18 Jan 80 | 1 | 1 | 23 40. 50 | Ş | ģ | | Ž, | 1 74 50 | Ì | Ì | | 16 Hay 80 | Ž | Ž | 23 Kay 80 | Ì. | 7 | | | Ę | ş | | | Ş. | 5 | 3 | Ŗ | 25. 25. | Ż, | Ŗ |
| Flight Mission Rumber | 2030 | 3712 | 3028 | 1014 | 3020 | 3012/3015 | | 5015 | 0101 | 9751 | 1010 | 1012 | 3012 | | ET SE | £ 5 | 200 | 2006/2010 | 200 | 5011 | 1015 | 1016 | 5014 | 202 | 2002 | 22 | 1010 | 1101 | 2015/12/16 | 3013 | 3014 | 0101 | 5012/5016 | 1010 | 2029 | 6704 | 300 | 4023 |

*Left Spoiler Only

~ id¥5 (#\$\delta\s)

APPENDIX B

RMS ACCELERATION AND SOUND PRESSURE LEVEL DATA

| Table B-1 | Overall RMS Levels Produced by Stabilized Flight Condition Listed in Table 3 |
|-----------|--|
| Table B-2 | Peak or Maximum RMS Levels Produced by Transient Flight Conditions Listed in Table 4 |

TABLE B-1

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

| | 777 | # | == | = | 1.11 | == | 1 | Ę | 22. | 2 | 1 | 9.1 | 2,96 | 2.2 | :: | = | = | = | = | = | . = | = | |
|------------------|---------|-------------|--------|-------------|--------|------------|--------|--------|------------------|--------|----------|-------------|--------|-------------|------------------|-------------|-------------|---|-------------|-------------|------------|------------|--|
| | 434 | 53 | z z | 27 | = | 7.5 | .85 | Ş | 37. | 2 | F. | r. | = | ė. | 27.5 | 7 | 1.11 | 2.40 | 7 | 7.2 | 7 | 7 | |
| | 1251 | 84. | 2,7 | Z. | 8 | 20. | 181 | * | . 20 | | * | 15. | 7. | 2. | 88 | R 1 | 2112 | 14 | 4 | ** | 919 | 213 | |
| | 7227 | 3 5. | 25, | Ą | 2 | 2,7 | 15. | 2 | ,25 | . 98 | 7. | 22. | 7. | ř. | 8.7 | | 111 | 5 | .= | 217 | 4 | 110 | |
| | 1881 | 3 8. | ¥, | | | 2,2 | 7. | 3 | .72 | | 3 | W. | 2. | 3. | 2,78 3,98 | 99.5 | 2.46 | 2.50 | 1 | 2,66 | .35 | .46 | |
| | #10 | 127,00 | 124,86 | 1,10 125,50 | 727 | 127,94 | 130,00 | 124,40 | 125.70 | | 127,30 | 5.69 122,26 | 123,00 | 9,68 127,88 | 130,00 | 6.20 127.20 | 8,66 134,56 | 6.20 127.40 | . 96 126.70 | 7,98 127,36 | .66 122,06 | 29 123, 90 | |
| | 1421 | 2,69 | 3,06 | 95.5 | 13.66 | 8 C 7 | 24.36 | | 2,10 | | 15.00 | 5.63 | | 9.6 | 7,60 | 6.20 | 99.9 | 6.70 | .= | 7.98 | 3 | | |
| | 7527 | ** | 1111 | z | \$ | 2,7 | 7 | 2 | 22. | 87 | 35. | z. | 7. | 8 | 15, 16 | 16,30 | 14.00 | 13.56 | 6.48 | 1.8 | 23 | :13 | |
| | 1231 | 22.12 | 55. | 1.27 | 2,0 | 22 | 3.00 | | 1,30 | 2.18 | 2,10 | = | 1,00 | 1,20 | 6,4 | 1,66 | 7.46 | 7.00 | = | 111 | = | | |
| | 1 | | 22, | | | 2 | 1,36 | | , 62 | 1,10 | 1.10 | 4 | 88. | 1.0 | 11,51 | 9, 58 | 12,38 | 11,00 | 5.5 | 13,76 | .39 | . 32 | |
| | 727 | | 25. | \$7 | 2 | . 5 | 111 | 7. | 97° | . 48 | = | æ, | 9 | .62 | 2.66 | 1.56 | 2.2 | ======================================= | = | 2,01 | 7 | 284 | |
| | 114 | 1.68 | 95 | | 1.38 | | 2.10 | = | 96 | 1.70 | 1.56 | 19. | .78 | = :- | 4.76 5.78 | 3,96 | 5.30 | 7.88 | 2.96 | 5.50 | .50 | 49. | |
| | PCC | 22 | 22 | 87 | -) | nn | 7 | n | 4 10 | i. | l | m | 5 | ï | 2.5 | = | i | = | 7 | į | × | • | |
| 10%1 | DATE | 119002 | 668527 | 384623 | 905456 | 120514 | 866519 | 200434 | 868913 868913 | 896428 | 185888 | 827968 | 98428 | 383428 | 808656 329559 | 10000 | 111679 | 300612 | 919900 | 129686 | 33000 | 96862E | |
| SHITCH POSITIONS | #135104 | 3213 | 3814 | 1916 | 29.18 | 2942 | 1816 | 3412 | 6782 | | 4786 | 1181 | 1101 | 1811 | 5619 | Seza | 1101 | 2815 | 1010 | 3012 | 3919 | 5412 | |
| SWETC | 70 8 | • | 2 | = | 13 | | 2. | 22 | | 72 | | 2 | 28 | 2 | 3 | | # | 7 | 5 | 2 | 2 | 93 | |

and the same of the same of the

TABLE 8-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

| - | | .38 .96 | | | | .90 2,58 | • | | 103 41 | | l | 10. 6 | | | 50 | | | 25. | 96 2,28 | 2.48 | | 40 4 40 | ł |
|------------------|----------|---------|-----------|-------|--------------|-------------|---|------------------|------------|--------|--------|---------|--------|--------|---------|-----------|---------------|----------|------------|---|-----------|---------|---|
| | | 910 | | | | | | | 181 181 | | 1.7 | .76 .27 | | - | 1 | 2,30 1.21 | H | | 90.1 | 1.30 1.10 | | , es | 1 |
| | | | | | | 7. | | - | 164 4 | | .15 | 8.5 | | | 3 | 1.26 2. | | | .78 1. | 1.00 | 1.20 2.00 | , | Ī |
| | . 40 | .37 | .35 | | 7 | 3. | | | 1414 | | | 7,7 | .41 | | 2 | 1.00 | N. | 3 | 1.30 | 1.2 2.1 | 1.44 | 17.4 | |
| | 124.00 | 123, 86 | 96 125,20 | 12% | 64 123, 88 | 9,48 125,48 | | | 1391 | | | 17.5 | 1.30 | 2.0 | 1.30 | 3,00 | 30.7 | | 1.46 | 2,73 | 2.80 | 1,10 | l |
| | | 7. | | 74 | 7 | • | | | 191 | 2.30 | | 98, | .32 | | 2.30 | 4.20 | 1,1 | | 2.78 | 2.44 | 216 | 1,24 | |
| | . | .12 | 41, | . 28 | -12 | 7. | | | 474 | 1.00 | | .36 | u | - | = | 1.66 | 3. | 7. | E . | ======================================= | 3 | .35 | |
| | 1.8 | == | 26. | . 71 | | 1.96 | | | 1481 | 25 | 2.00 | 35 | .38 | 20 | | 2,36 | F.: | R. | 1,9 | 2.2 | 1.69 | 1.8 | |
| | | Ä | ķ, | .28 | .28 | 3. | | · | ASSA | 5,66 | 2 | , 52 | | 3, E | 2.0 | 5.36 | 337 | 1.78 | 21.3 | 5, 5 8, 28 | 2,80 | 1,30 | |
| | 9 | , Y | 5 | e Pi | . 29 | 8. | | | 1221 | 1.10 | 27. | SK. | | 1.16 | Ę | 2,00 | 2,5 | = | 3. | 2,7 | × | .86 | |
| | . 28 | | | .53 | 35. | 1.10 | | | AZEA | 1.20 | .71 | S, S, | \$ | | = | 2.86 | 2,2 | = | r. | # 55 # 55 | 1.78 | 19 | |
| | | nn | ~ | n | Pa | • | | ~ | 7 | 7 | 22 | - | 4 | • | • | - | - | - | - | 2.7 | 2 | * | |
| Ibrie | 1,196.56 | 304616 | 319141 | 19868 | 310000 | 115948 | | SALTCH POSTTIONS | PATE SEC | 915388 | 119636 | 869523 | 542423 | 986986 | \$15292 | 615029 | 664436 | \$150613 | 986425 | 196428 199981 | 984421 | 827988 | |
| SHITCH POSITIONS | 6106 | 101 | 50.50 | 1101 | 200 | 2005 | | 1864 H3 | TC HISSICH | 1016 | 3013 | 2314 | 311 | 2698 | 1015 | 9101 | 3012 | 1949 | 1915 | 4786 | 1612 | 1011 | |
| | 12 | ļ | = | • | | - | | SALT | 2 | ^ | | 63 | = | 13 | | ž | E. | | R | 2 | N | 2 | |

TABLE B-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

| | A224 A224 | | YEAY | 7277 | • | | , | • • • • | • | • | | |
|-----------------------------|-----------|---------------|------------|-------|------|-----------|------|---------|------|-------|------|-----|
| 100656 100654 100654 | | | | | | 494 | 4394 | | 3 | | 484 | 2 |
| 909450 | 99 4 | 6.28 | 5.38 | | 1.70 | 26.1 | | | 2.66 | * | 3 | 1 |
| 987616 | | 9.9 | 3. | 7.20 | 2.36 | 2.16 | 3.6 | P | 2.6 | 7. | 2.18 | |
| | 4.58 | 4.78 | 8 . | 3.68 | 1.50 | 1.29 | 3,78 | 3.9 | 1.0 | 3,50 | 1.56 | 2 |
| 1818 838689 20 | 96", | 4.56 | 2.68 | 7.06 | 1.78 | 1.36 | 1,31 | 9,48 | 2.20 | 2.4 | 1.71 | |
| 2715 888618 24 | 3,40 | • | 3,46 | 3,20 | 1.36 | 1.34 | 2,10 | 2.0 | 7. | 2.8 | 1.3 | 2 |
| 1815 308616 22 | 3,41 | 2,88 | 3,36 | 1.80 | 1.28 | 1.16 | 3.78 | 3,36 | 1.28 | 2,3 | 1.28 | |
| 5812 888628 16 | 64.70 | 4.36 | 2,6 | 7.86 | 1.46 | 1.30 | 3,63 | 7.4 | 2.10 | 7, 28 | 1.46 | |
| 5819 886685 2C | 77. | 22. | .36 | .26 | = | = | * | 7. | × | 3 | Z. | • |
| 5612 8665,46 | er. 5 | 12. | ₹. | 97. | .23 | 25. | 7. | 7. | 7. | 2. | 25. | 3. |
| 2915 898618 | 62. | 3. | .28 | 18. | 51. | . 16 | .20 | 2. | 7. | 2. | 93. | • |
| 5859 886686 1516 888686 | | 5.2 | ₹,₹ | 7. 7. | 2.5 | 2: | 7.5 | 2.5 | 3.7 | 2.5 | z: | =: |
| - | | .27 | 25. | 25. | . 12 | 22. | .36 | * | = | 2 | | |
| 5624 668686 | 87. 8 | | | .78 | 2. | .23 | 5 | 1 | 5. | | .26 | į |
| 1811 \$80689 513 \$80689 | 85 F | 7,7 | 1,28 | 1,24 | 17. | 21.0 | 2,5 | 27,1 | £,r, | 5E, | 2.00 | 100 |
| 91 2046 400513 10 | | .00 2,50 1.00 | 2,36 | 10.7 | | 8,34 1,3g | 1,3 | .28 | | 1.8 | | Ţ |

| Sull | CH P953 | Switch Position, S. | - | | | | | | | | | | | | |
|------|--------------|--------------------------------|------------|--|-------------|-------------|--|------|------|---|--------|------------|-----|------|-----|
| J | HTSSION | 5472 | 7 | TE HTSSIQH BATE NEC ASÍA A36A B34 B20 A43A A44A B3M B2M A34A A380 439A E6A | 1361 | | 124 | 4434 | 1441 | 2 | 120 | 4344 | 187 | 1351 | EGA |
| | 1816 | 1000319 | 2 | 7 1816 886519 25 108 108 24,00 448 25,36 109, 64, 69 185 186 1 | 11 | | 24, 80 | 448 | 2.30 | | 2 | | ş | 7 | *** |
| | 2813 | 119999 | 7.2 | 99. | .76 | 10"9 | • | \$8. | .7E | 2 | 141.00 | 3 | 3. | 23. | = |
| | 5e14 5e14 | 5814 888523 5 5814 886523 6 | n • | . 24 | 3 12 | | 24 . 54 . 64 4. 66 . 64 . 65 . 65 . 65 . | 2,2 | 25 | 3 | 37.55 | 3 : | 2. | 8: | =: |
| | 3814 | 119288 | s n | | .66 | 8 .∼ | .76 | .20 | . 22 | 2 | 35,00 | = | = | = | |
| _ | 1818 | 881623 | ~ | 18, 18, 19, 19, 10, 10, 10, 12, 12, 12, 14, 16, 16, 16, 16, 18, 18, 18, 18, 18, 18, 18, 18, 18, 18 | 20. | 2.00 | 1.30 | .28 | 25. | 2 | | 65. | R. | 22. | 1 |

TABLE 8-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

| | 181 | 3,28 | 2 | | ä | = | 2.01 | 2.56 | 67.5 | 1.38 | 1.48 | 181 | = | ĘĘ | 3 | = | 8 | 2 | 3 | 8 | = | 33 | | 1 | i i | 3.46 |
|----------|---------|----------|-------|-------|--------|--------|--------|--------|--------|--------------------|--------------------|---------------|--------|------------|--------------------|-----------|--------|-----------|-----------|--------|--------|------------------|--------------------|------------|------------|--------|
| | 1351 | 3. | | • | 1.28 | = | 25. | 5: | = | | | H | 3 | | 1.66 | 114 | 81 | 9 | * | 2 | 8 | Ŗ | 2 | ; | = | 3. |
| | 1381 | 3 | | ř | 1.26 | 7. | 3. | 7,3 | 55 | 39 | 18 | 87 | 999 | 77 | 27 | 111 | 224 | 7 | X | = | Ž | z z | * | | z. | 4 |
| | 1341 | 3. | | | | 3. | 29. | 2.3 | | 22. | .32 | . 39 | 70. | === | 1.88 | 97 | 121 | 113 | \$1 | . 10 | -114 | 21. | 22. | | Ħ. | 7. |
| | 22 | 139,38 | 3 | | 161.00 | 156,86 | = | 23 | 193,44 | 24.58 | 55.00 | 51,18 | 8 | 2.5 | 35,48 | PR 152.99 | | 40 135,30 | ne 139,39 | 133,10 | 132,46 | £ 5 | 32.70 | | 135.80 | 156,80 |
| | 2 | 3 | | | 145,66 | 131,20 | 3 | 131,00 | | 1,10 127,60 154,59 | 1,18 128,98 155,88 | 126,22 151,11 | 8 | . = | 1,46 145,96 195,46 | i | 142,00 | 26 135,48 | 136,00 | 136,00 | 2 | 134.18 | 26 127, ps 132, 70 | 128.00 | 129.00 | 8 |
| | 1144 | 2.2 | 207 | | 1 11.7 | 1.36 | 1.84 | 2.38 | 2 | . Brit | 110 | | 2,26 | N 10 | 1.0 | 2 | 2.88 | 188 | | 2 | | 2.6 | 25. | | 22. | 1.78 |
| | 1431 | 3 | | | 7 | 57. | \$ | 3.5 | 3 | 120 | . 25 | K | 3 | 2.5 | 2 | 1.25 | 1,28 | 12. | 2 | 12. | 1 | ฎผู | 1 | .11 | z. | 7 |
| | 124 | 27,46 | | | 52,48 | 16.00 | 21.46 | 24,48 | 17.88 | 6.78 | 9. 30 | 10,00 | 15.00 | 2.2 | 12,00 | 16, 50 | 11.00 | | 111 | | 1,10 | | 1,13 | 3 | 1.0 | 21.50 |
| | 134 | 2,8 | , | 1 | 19,60 | 2,10 | 7.61 | | 5,'68 | 3,2 | 3,00 | 3,88 | 6.23 | | 7,48 | 97,9 | 97.9 | 1,18 | 3 | 3 | 1.78 | 3 3 | 2,48 | 2.3 | 1.26 | 3.46 |
| | 1361 | 2.2 | | | 2,00 | 3 | ** | 26. | 2 | 97 | 35 | 9 | 3 | 2.2 | 9 | 1.39 | 3 | 11 | = | 2 | 22 | 7. 7. | 32 | 22 | Si. | . 15 |
| | 4514 | 3 | 20 | | 1.40 | 3 | = | 9 | | .57 | 53 | | 2,61 | 27.2 | 1.36 | 1.56 | .= | 72. | .5 | 2 | 25.0 | 72, | 80. | 32 | .24 | = |
| | EC. | S | | n | | S | 50 | Ç, | 2 | 5 | 2 | Z | 12 | 22 | 12 | ŝ | ij | 37 | 4 | 8 | ı | an an | 7 | u 1 | e 1 | = |
| 186 | PASE | 985888 | 11021 | 77624 | 615969 | 198434 | 388423 | 866428 | 100422 | 186428 | 857888 | 127891 | 757631 | 110617 | 80000 | 888616 | 529628 | 989686 | 0A862# | #190J9 | 200208 | 888689 888616 | 929449 | 535649 | 808611 | 868513 |
| POSITION | HYSSION | 2868 | 1 | 32.79 | 1916 | 2015 | 1612 | 1912 | 1612 | 1811 | 1811 | 1015 | - 1 | 1811 | 1016 | 1516 | 5012 | 5019 | 5612 | 2115 | , | 1818 | 5829 | | , | 2886 |
| SHITCH | TC H | 1.0 | | | 21 | 22 | ม | 72 | n | a | 2 | 2 | = | | 2 | 3 | .5 | 2 | 2 | = | 187 | | 2 | • | | 2 |

TABLE 8-1 (Continued)

原体的特別的政権的情報を表現する。 まんしん かんしょうかい しんめん (物質の) かんかん なんない しゅうしゅう しゅうしゅうしゅう いんしょう かんしょう しゅうしょう しんしょうしょう

1

.

| | | 107 | - | | = | | 3,10 | === | : | 2.5 | 2.0 | | 2.61 | | 1.30 | 1.6 | 2,01 | | | = | = | 6. | = | | #: |
|-------------------------------|----------------|---------|--------|--------|-------------|--------|----------|----------|--------|--|--------|--------|--------|--------|--------------|--------|--------|--|----------|--------|-----------|--------|--------|--------|---|
| | 1 | 4104 | 143 | 36. | 27. | .23 | 1:0 | 25. | 2,10 | 2.5 | | | === | 1.30 | 3. | 38. | 7. | 3,76 | 3.9 | 3,48 | = | Ä | .16 | 2. | |
| | | 7587 | 112 | 717 | 3. | = | 38. | 77. | 4.1 | 2.2 | 38 | 96 | ž | .23 | 25. | 25. | 2. | 150 | is. | 99. | E | == | .10 | 2 | |
| = | | 1244 | \$1 | | = | = | 25 | 22. | \$ | 2.2 | Ä | 5 | 7. | 2. | 2 | 2 | 25. | 68. | 3 | S. | 19. | = | | 45 | |
| STABILIZED FLIGHT | | 1104 | 181 | | .24 | z. | 1,36 | 37. | 2,66 | 2,2 | 1,20 | 100 | 1,48 | 1.48 | 7. | H. | 1.50 | 3, | 5 S | 5,30 | 12. | 7. | ä | 7: | 2 |
| SILIZEI | | 4134 | .76 | .73 | .26 | ř. | 2,36 | 2.63 | 9.7 | 22 | 2,99 | 2,58 | 3.00 | 2,30 | 1.22 | 1.4 | 1.48 | 2 0 | 2.2 | 1,98 | Z. | z. | 2 | 23 | 2 |
| | | 4164 | 79. | 1.50 | 95 , | 7 | 5.18 | | 11.48 | 2,7 | 4.88 | 5.98 | 6.28 | 8.48 | 2.78 | 3.85 | 3,48 | 3.50 | | 3.11 | u. | ₹. | .28 | 8, | Ä |
| PRODUCED BY | | 4154 | 1.10 | | 7 | . 92 | 2.0 | 2,19 | 5.00 | 2 5 2 5 2 5 2 5 3 5 4 5 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 | 25. | 2,10 | 2.28 | 2,18 | = | 1.00 | 1.18 | 7.68 | N 9 | 4.48 | 49. | ₹. | .4 | 5 | 3 |
| S PROF | | 1331 | i. | | ï | ₽. | .20 | 2 | .20 | =:- | 91, | .26 | 121 | . 25 | 51. | .28 | ₹. | 75. | • | 7. | Ę | 3. | | - | = |
| OVERALL RMS LEVELS PRODUCED I | | 1374 | 1,30 | 38 | 97 | 3 | | 2.5 | 5,13 | 2.5 | 2,88 | 3,28 | 3,28 | 4.18 | 7 | 1.70 | 2.2 | 2 7 | 8.28 | 5.26 | ₹. | 25. | 2 | | ġ. |
| ALL RM ITIONS | | 4124 | 2.28 | 1.1 | | 1.62 | 3, | | 7.48 | 2,38 | 5,68 | 4,58 | 19"7 | 7.10 | 86. 1 | 2,46 | 3,88 | 10 00 00 00 00 00 00 00 00 00 00 00 00 0 | 7 | ¥. | " | = | 99. | 30, | 29 |
| COND | | ASIA | 1.56 | 3 | . 48 | 3. | 1,40 | 25. | 2.48 | 26 | 1.20 | 1,78 | 1.58 | 1.98 | 95. | = | 1.1 | 2.00 | 3.38 | 2.73 | 35 | | 65. | 47 | ž. |
| , | - | 32 | 1 | • | • | - | • . | - | • | 7 | • | 18 | • | 3 | • | = | × | 22.5 E E | 2 | • | 2 | | • | • | • |
| | | 2170 | 89862# | 168523 | | 819623 | 890586 | 086527 | 198519 | 88843# 886581 | 106428 | 826428 | 185889 | 127981 | 331428 | 127988 | 896428 | 109000 | 129449 | 199616 | 99911 | 179966 | #198fe | 759265 | 0.0 0 1 1 E |
| | BELLEN FORTING | HTSSION | 5012 | 5914 | 3814 | 101 | 2308 | | 1816 | 3853 | 1012 | 1812 | 7847 | 1112 | 1181 | 11811 | 1181 | 5919 | 5812 | 1919 | 6186 | 5812 | 2015 | 5019 | ======================================= |
| | 3110 | 2 | • | 17 | ! | = | S | | ž | 22 | 2 | 72 | | X | a | 22 | 2 | . | | 9 | | = | • | 4 | |

TABLE B-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

SHITCH POSITIONS

| E64 | 3 | = = | 3.56 | | £134 | = | | I. | = | 37,00 | | ä | 3: | 36.08 | 3.18 | 21,60 | 72,10 | 17.00 | 26.88 | 38,26 | = | |
|---------|-------|------------|--------|-----------------|------------|--------|--------|--------|--------|--------|--------|--------|--------------|--------|--------|--------|---------------|--------|--------|--------|---------|--------|
| 181 | .22 | 24. | .79 | | £61 | 994 | . 82 | 11. | 1,53 | 1.00 | 20°1 | 1.70 | 3: | 1 | | .71. | 1.40 7 | . 32. | 5. | .56 | 1.38 | # # P |
| 1284 | | 2,5 | 34 | | 6121 | 2 | 91 | .10 | 11. | 21. | .25 | 41. | 9: | = | 23. | 97. | 11. | i. | 91. | 7. | 3. | 3 |
| 1144 | = | 2,7 | .2 | | EZA | 93,20 | 95,56 | 45,00 | 74.58 | 96.36 | 85.88 | 47.28 | 3: | | 67,20 | : | 77.98 | 43.66 | \$2.28 | 47.28 | 119.16 | 104.28 |
| 1194 | × | 77. | | | 110 | 121 | ,17 | .13 | 13. | 954 | 1 | K. | 20,0 | | . 56 | .53 | 25. | ž. | 7. | × | 1 15.7 | |
| 4534 | 7. | z z | 1 | | 1610 | | . 87 | = | .0. | 2 | | .15 | 2,5 | | .11 | 3. | = | = | =: | | 1.50 | 2.28 |
| 4164 | 7. | 5.5 | 4.00 | | £124 | 3 | 11,40 | 4.18 | 5,36 | 20,66 | 21.38 | 35.00 | 12.00 | 15,48 | 21,00 | 23,88 | 17.10 | 9.0 | 12.00 | 11.88 | 7.7 | 7.7 |
| A15A | 5. | 7.5 | 3 | | D144 | . 18 | .16 | = | -12 | .28 | 2. | .28 | 370 | .12 | 91. | .13 | .16 | 9. | 2. | 17. | 56 | 99 |
| 4334 | =, | 3.5 | = | | B 5 K | .= | | 2 | | 38,88 | 139.00 | • | 135,12 | = | | 138,38 | 142,80 | 135,88 | 136,48 | 138,98 | 168,80 | 168.20 |
| A37A | 3 | 2, 3 | 2,16 | | B6N | 122,58 | 124,38 | | | | | 141.10 | 148,88 | 137,18 | 139,81 | | 141,28 142,80 | = | 135,46 | 130,28 | 1 .07.1 | |
| V217 | SI. | 99 | 2.98 | | 964 | 3,68 | 883 | ř. | 1,23 | 2: | 4 | 6,18 | 2,28 | = | 11 | 10.1 | | 1.78 | 2,28 | 7,4 | | 38.85 |
| A11A | .46 | 9. | 1,10 | | 154 | 3,28 | 76 | , | 1.23 | 3,10 | 3.5 | 6.1 | 1.98 | 2,68 | 3,68 | 3.69 | 5.10 | 2,28 | 2.48 | 3,38 | 27,50 | 29.78 |
| נב | 100 | • | 25 | | i i | 2 | | _ | • | | | • | w m | - | 83 | 1 | Si. | - | 2 | 22 | 7. 5 | = |
| DATE | 98988 | 888689 | 000513 | TOWI | 2746 | 129888 | 166523 | 219889 | 888623 | 848586 | 888527 | 888519 | 888438 | 888428 | 868428 | 888288 | 698428 | 888428 | 888428 | 106428 | 38686 | 896628 |
| MTSSIEW | \$626 | 1011 | 2816 | SHITCH POSITION | TC MISSION | 5812 | 3814 | 2814 | 1010 | 2938 | 27.82 | 1916 | 3815 4785 | 1012 | 1812 | 4786 | 1812 | 1811 | 1881 | 1181 | 5819 | 5812 |
| 4 | = | : . | | SMIT | | • | .5; | | = | 2 | | i. | 22 | 2 | 2 | | 92 | 23 | 77 | 52 | 9 | |

. william

TABLE B-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

| - | 1111 | = | = | = | = | = | 7.5 | : | = | == | 15-72 |
|---|--|---|--|---|---|--|---|--------|--|--|---|
| | 787 | 1.36 | ×. | 1.23 | 1.2 | 3. | 3.2 | - 12 | 5 | 3.5 | |
| | 1210 | 3. | 7. | = | #. | 1 | 3.5 | | = | 7.7 | 8 |
| | 123 | 01.48 | 11.81 | 78.38 | 77.88 | 70,70 | 96.48 | 45,18 | 48.60 | 46.89 97.88 | 63.26 |
| - | 110 | 2,76 | 2,70 | 97. | 57 | 113 | £ 7. | EJ. | R. | 25 | • |
| | 1124 | .62 | = | | E . | . | 2,2 | | ä. | | |
| | 2213 | 16.7 | 5.78 | 3,6 | 1.36 | 17.7 | 3,78 | 4.78 | 19.7 | 3,26 | 16,99 |
| | 0144 | 3 | 9. | 37. | .12 | = | == | 111 | = | 7,5 | . 13 |
| | 18 | 45.48 | 3. | | 19.62 | = | . 91 . 58 . 46 . 18 . 62 118, 68 . 48 . 18 | 122,88 | 133,80 | 22 | .55 <u>.</u> F.6 |
| | ¥9 | | 138,78 | 126.68 | 11.011 | 3 | 110,011 | 117,38 | 119,96 | 117.00 | 130,66 |
| | 191 | 21,48 | 29.78 | 1.0 | 1.48 | .58 | | | | 3.5 | 2.28 |
| | 154 | 19.86 | 26.86 | 1.88 | 1.26 | 35. | 9.5 | = | 1.01 | 7.02 | 1,00 |
| | P.C. | = | 2 | 52 | | • | ~ ~ | • | • | | iz. |
| | DATE | 199111 | 838616 | 889888 | 5112 886628 E 1.28 1.48 119,18 129,68 ,12 4,3E ,69 ,15 77,88 ,11 1,28 ,68 | 2315 686518 7 .54 .58 .88 .06 .18 4.48 .18 .15 76,76 .10 .00 | 500000 900000 | 888616 | 75968 | 1611 808589 7 62 63 68 88 88 18 3,28 718 65,89 6.11 668 581 881 881 881 881 881 881 881 881 88 | 889513 |
| # TOTAL CO. L. C. | TE HISSION DATE FRE 854 864 864 814 8124 BISA BISA BIL EZA DIZA E64 E134 | 63 1811 88669 19 19,06 21,48 .88 145,48 .68 4,98 .62 2,78 181.48 .33 1,36 | 66 1019 3aB614 17 26.08 29,78 138,78 .89 .46 5,78 .08 2,79 85,18 .45 .94 | 64 5819 88888 29 1.78 1.88 128.88 .84 3.68 .87 .16 78.38 .18 1.28 | 5812 | 2315 | 5019 884694 7 .89 leif 888685 7 .81 | 1818 | 55 5528 5858 6 1.88 1.98 119.88 135.88 .08 4.88 .98 .28 48 65.68 .18 .85 | 100 | 98 2886 519513 is 1,98 2,28 139,88 135,80 ,15 15,90 ,89 ,48 63,29 ,80 ,10 27,81 |
| 1 | 16. | 65 | 90 | 3 | 5 | * | 23 | | S | = | |

| TÉ MISSION DATE NYE BYN BBN BBA BILAS BISAR BYN BIRA BON BIRA BIRA | 7 Seiz 88862# 22 142,98 ,88 3,18 3,99 1,98 2,18 143,68 ,88 5,68 17,88 136,88 ,88 | 8 1816 888519 17 143,18 141,18 4,48 5,88 2,78 7,88 142,28 154,68 5,88 7,88 135,68 ,80 | 17 5414 888523 9 "88 137 88 1,78 1,78 65 2,58 135,88 154,19 1,88 4,89 128,88 468 154,19 1,88 4,89 128,88 468 | | 10 1818 889023 18 . 44 2.58 2.28 1.84 1.24 . 96 . 96 3.48 126,38 . 96 . 96 | 19 2008 902506 8 142.88 141,08 5,88 1,28 5,88 00 159,09 12,88 154,09 16,48 18,88 156,48 18,48 18,48 18,48 | = | Zi 1816 543519 6 147.98 .84 5.86 5.86 9.86 9.98 142,28 156,86 7,89 17,78 138,38 .88 | 27 3853 888434 \$ 136,14 98 2,88 3,10 74 2,88 136,38 131,88 2,88 5,38 60 60 | 11.11 |
|--|--|---|--|----------|--|---|----------|---|---|-----------|
| 804 8 | 17,88 138 | 7,68 135 | 4.69 128 | 7,88 125 | 12,18 130 | 12,68 134 | 4,18 134 | 17,78 138 | 5.30 | 5.26 (35. |
| 910 | 5.64 | 5.60 | 1.00 | | 37.6 | 2.4 | 7.7 | 7.39 | 2.54 | 2.48 |
| 1 | | 154,00 | 154,10 | | 31. | 159, 88 | 152.98 | 156,96 | 131.00 | = |
| 818 | 143,88 | 142,28 | 135,86 | 2007 | 1 | == | Ħ, | 142,28 | 130,34 | 131.0 |
| 81142 | 2:10 | 7.00 | 2,50 | | 1.24 | E 2 | 5,48 | 9.9 | 2,40 | |
| B15A1 | 1.0 | 2,76 | 3 | | 1.04 | 2.5 | 1.36 | 3.66 | 72 | 7. |
| 87.4 | 3, 98 | 5.86 | | | 2.2 | 2, N | 4,18 | 9.00 | 3,10 | N. |
| 88 | 3,10 | 4.4 | .; | | 2.3 | 2 E | 13,18 | 31.2 | 2 | 7 |
| 1 | | 141.10 | 137,88 | | | 141. | 141.00 | 2 | | |
| - X | 142.98 | 143.18 | | | | 142,66 | 142.88 | 147.86 | 136,19 | |
| 2 | 2 | 17 | | • | | 50 60 | • | 45 | * | • |
| TÈ HISSION BATE NEC | 89962# | 868519 | 889523 | | 529849 | 901286 | .881527 | 615602 | 100434 | 12020 |
| HTSSION | 5#12 | 1016 | 5814 | | 1818 | 2088 | 2782 | 1816 | 2013 | 4/83 |
| 12 | | • | 5 | | 2 | £ | , | 12 | 2 | |

TABLE B-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

| - | 1214 | 1.4 | 17,58 | 12,75 | = | 19,60 | | = | į | | = | 38, | = | | = | | . | |
|----------------------------|---------|-------------|------------------|---------------------|---------------|-------------|--------------------|------------------|--------------------|---------------|--------------------|-------------|----------|-------------------|------------|------------|------------|------------|
| | KE13 | 11.10 | 136.00 | | 1 | 1 | | 93 | 12,46 | 36.15 | 29.66 | 33,06 | 7. | 121.68 | 128,58 | 130,50 | | |
| | 768 | 7,46 151,18 | 12,36 1 | | 3,88 125,08 | 6,58 128,96 | 9,48 122,88 | 9, 94 129, 90 | 16.86 132,46 | 7,86 128,36 | 9,16 129,66 | 4,28 133,08 | 7.SE 0 | 9.00 121.60 | | 7,00 13 | 8.65 129.8 | |
| | 818A | 3.40 | 5.56 | 7.28 | 2,49 | 1,38 | 4.39 | | 4.48 | 2,68 | 2, 66 | 2,00 | 2,34 | l | 2.48 | | 2.88 | |
| | 1 | | 154,48 | Ì | | | | ŀ | - 1 | | | | | 145.86 | 1 | | . } | |
| | B.5 BH | 131,00 | 135,89 15 | 5, 86 15 | .89 147,88 | .68 156,00 | 1,66 15 | 64 136,36 152,28 | 15, 86 15 | 135,29 145,80 | 4,68 14 | 131,06 | 12,18 14 | 132,00 14 | | 200 344,00 | 148.861 | |
| | 81162 | 4,08 13 | 6.48 13 | 18.88 135,88 155,88 | | 6, 10 | 5,78 128,68 152,50 | .64 13 | 2,08 138,86 154,36 | .94 13 | 1.00 134,68 147,10 | .78 13 | .87 13 | | .62 12 | | | |
| ر ب | 811A1 B | 1.18 | 2,10 | 3.86 | • | 1.00 | 1.66 | | 2,10 | | | . 52 | .78 | , ø. | .76 | 2.1 | | |
| N IAB | 174 | 4,58 | 6,98 | | 2,88 | 3,86 | 99,7 | 34,38 | 35,38 | 1.78 | 1,00 | 1.28 | 2,00 | 1,78 | 2,86 | ı | | |
| SIED | ¥88 | 27.48 | 3, 48 3, 68 | | 2, 86 | 2,28 | 3,10 | 5.86 3 | 5,48 3 | 1,89 | 2,18 | 1,48 | | 1,98 2,18 | 2,00 | 85.1 | i | # T " Y |
| CES | ¥ | • | 138,88 | 3. | } | | = | - 1 | 100 | | l | 2 | | 134,98 | | - | | _ |
| SONDITIONS FISIED IN IMPLE | 87# | 139.00 | 141,48 13 | | 131,0e 132,00 | 134.00 | 136.38 | . 02 141 88 | 30. | .88 136,88 | . 00 136,66 | = | | .88 13 | .00 132,00 | 106 132,06 | | 77 BB###71 |
| | 1 | • | 2 - | 32 | - | 28 | 36 | 4 | 52 | 25 | • | • | • | 10 10 | • | • | - 1 | |
| 1,0 | DATE | 127101 | 818428 886581 | 888428 | 686428 | 818428 | 688428 | 99998 | 669616 | 2022 | 994628 | 984618 | 58888 | 3696.89 898616 | 388688 | 300629 | 20061 | 147111 |
| SHITCH POSITIONS | HISSION | 1812 | 1812 | 1812 | 1911 | 1111 | 1101 | 5828 | 1910 | 5819 | 5812 | 2015 | 5819 | | 562F | | - 1 | |
| SHITC | Te HI | 23 | | 22 | 27 | 28 | 52 | 9 | 3 | 2 | 5 | 2 | 87 | | = | = | | |

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TABLE 8-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

SHITCH POSITIONS

| 1 3 | = | 릨 | • | | | 77.77 | | : | | 93 86 | | 210 | 22,11 | | | 27.60 | 28.85 | = | = | : | | = | | : | | | 86,48 |
|---------|---------------|----------------|--------------|-------------|--------|--------|---------------|---------------------|---------------|--------------|--------------|--------|---------------|---------------|---------------|---------------|---------------------|-------------|-------------|-------------|-------------|--------------------|---------|---------------|--------|-------------|---------------|
| 6114 | 6.88 | 4 | 2,88 | | | 3 | | ; | | | | | 2.5 | | 1 | 1 | 5.6 | 2 | | | | 3 : | | 9 | | 2.5 | 1,5 |
| 8154 | 7.80 | = | 2,66 | | | | 5.28 | | | | | | Ŗ; | 2.5 | | | 3.48 | 7.66 | 2,50 | | | | 3.00 | 3,66 | | 2.3 | 15. |
| 1918 | 11,00 | 10.11 | 41.46 | 58.48 | : (| | 50.00 | 27 46 | | 29.62 | 39.00 | | 7 | | 16.0 | 15,88 | 9,28 | 16.31 | 36,88 | 17 17 | | | 41.18 | 59,48 | | 39.65 | \$2.06 |
| 815r | | 135,00 | .= | , 88 | | | 134.28 | 133, 20 | | 8 | | | 133,00 | 134.00 | | 136,88 | 134.84 | = | EF 133.00 | | | 2 2 | 132, 56 | | | | 41.66 |
| 8184 | | 49 172,84 | 178,18 | 4.58 167,08 | | | 21.49 175 18 | 34,86 152,48 133,86 | | 161.18 | 3, | | 154.26 | 17,06 150,00 | 86 155, 98 | 13.88 151.80 | 10,00 153,00 134,00 | 169,28 | | 3,58 159,26 | | 3.96 163.18 124.28 | 164.56 | 4. 89 162, 39 | 157. | | 173.68 141.60 |
| E121 | 8.28 | 24,48 | 11.38 178.18 | 4.58 | | 18. | 21.48 | 34,66 | ,,, | Ŧ | 16.86 | | 22.88 | 17.06 | | 13.66 | 18,00 | 97.7 | 3.72 | 5.56 | | 2.98 | 187 | | | 7 | 16.99 |
| EZH | 4.40 144.90 | 129,00 | 1.98 133,48 | 2.42 135.88 | | 38.08 | 4-48 143.00 | 134.66 | 00.021.00.71 | 14.68 136.08 | 16.48 141.68 | 7.5 | 141.00 | 8,78 139,06 | 134.86 | 10,69 146,68 | 132.00 | 2.6F 133.8g | 1.88 135.88 | 1,58 138,88 | 2.68 148 88 | 136.48 | 136.88 | 2,48 136,86 | 132,66 | 1.56 132.00 | 137,58 |
| 15.34 | 4.40 | 32, 98 129, 88 | 1.98 | 2.42 | | 18.8 | 47 | 18,88 134,88 | | 14.68 | 16,48 | | 12,88 | 8,78 | 18.00 | 18,69 | 11.4P.132.PE | 2.66 | 1.81 | 1.58 | . 6 | 2.30 | 5 | 2.48 | 1.78 | 1.56 | 12,18 |
| Bish | 44,18 | 14,60 | 4,66 | 2,38 | , | | 3,16 | 4,88 | | 1.7 | | 2.40 | 3,28 | 3,68 | 5,89 | 10,98 | 4,68 | 37,7 | 4,38 | 1,10 | . S. | 2.38 | 2.48 | 1.1 | 2, 10 | 2.80 | 3,28 |
| B14H | 145.08 | P 146,88 | = | . 88 | | | 139.00 | | 6 4 K C | = | 135,88 | 62.0 | 34.60 | 146,00 | 132,88 | 135.88 | 143,00 | = | = | | = | = | | = | | = | 143,88 |
| BISH | 132,00 145,00 | 147.00 | | -Br | 135.46 | 138.28 | 133.88 139.88 | 144.48 | 141,48 (15,18 | 148.88 | 139.18 | 16 67 | 144,88 134,88 | 142,88 146,88 | 137,88 132,88 | 141,38 135,98 | 142,08 143,FB | 15 134.00 | . 88 | . 88 | | - 96 | | | . en | 2 | 135.38 |
| REC | 2 | , | = | = | 4 | • | ٩ | 9 | • | - | • | 1 | ;0 | z | • | 7 | 22 | 12 | 7 | • | • | 6 | ٦ | • | • | • | 2 |
| DATE | \$\$862E | 600519 | 006523 | BRAGIT | 596586 | 684519 | B68527_ | 868519 | 88643# | 388281 | 39A428 | B9F428 | 80.6561 | 888428 | 35428 | 868428 | 888428 | 588686 | 885586 | 989618 | 888688 | 639861 | 889616 | 889686 | 885589 | 898611 | 888513 |
| HISSIDN | 5812 | 1816 | 5814 | 5614 | | 5183 | 2782 | 1816 | 3813 | | 1612 | 1 | 4786 | 1012 | 1911 | 1611 | 1811 | 5626 | 5819 | 2815 | 5819 | 1818 | | 5828 | 1811 | 3813 | 2002 |
| 1 | - | - | - | * | 19 | | | , <u>z</u> | 22 | | ม | 77 | | 23 | 22 | 28 | 62 | 9 | 2 | 2 | 5 | | | = | 83 | | |

TABLE B-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

SHITCH POSITIONS

| 2114 | | = | 142.88 | | 8 | : | 8. | 131,50 131,00 | 142.88 | 7.88 | 138.98 138.68 147.88 | . 68 132. 88 148.18 143.88 149.38 148.48 141.38 142.19 141.88 151.88 | 68 119'88 121'88 129'88 128'88 125'89 129'88 129'88 129,88 13. 4b. | 124. R.7 129. 88 123. 28 124. 88 132. 88 133. 88 132. 88 132. 88 133. 88 131. 88 142.88 | . 68 125, 88 134, 88 137, 88 135, 18 135, 18 136, 88 135, 68 134, 88 145, 88 | = | = | | | == | = | : | = | 548,68 |
|---------|--------------------------------|---------------------------------|---|---------------|--------------------------------|--------|-----------------------------|-----------------------------|---------------|--------|----------------------|--|--|---|--|--------------------------------------|--------------------------------|----------------------|---------------|--|---------------------------------|---------------|----------------------------------|-------------|
| - | | | | | | _ | = | 7= | | 13 | | 3 | 3 | E | 7 | | | ┆ | _ | | | _ | | |
| CIEN | 86 129.50 | .88 127.88 | AR 135.00 | 135.60 | 98 148.28 | | 150.00 | | 134,88 | 137.83 | 9 | = | 3 | 3 | 3 | 146,58 | 98 128.81 | 98 126,89 | 68 127.88 | .BE 128.85 | BP 128.00 | 461 461 | 26.02 | 131.58 |
| | 12 | 72 | | | 3 | | 2 | 72 | 2 | 15 | 4 | 7 | 7 | 3 | 3 | 7 | 힉 | 77 | 123 | 121 | 2 | Š | 4 | 12 |
| CZH | 2 | = | 136.88 | | | • | | 127 181 181 | 134,88 | | 튁 | 뒥 | = | = | ą | 4 | 뒥 | 릨 | | 2 8 | 팈 | 2 | 4 | 3 |
| | Ì | Ì | 2 | | | ř | 12 | 32 | 13. | 138,86 | 138 | 42 | 욌 | 3 | 37 | 1 |] | I | | | | |] | |
| H87 | 3 | | | | | | | | 30 | | | 2 | | | | | Ę | 5 | 5 | 8.5 | | | | = |
| ٦ | - 1 | 1 | 135.98 | • | • | 5 | 20 | 18 | 133.30 | 38. | N | - | 29. | 3 | 36. | • 1 | 1 | | • | a r. | 1 | • | 1. | ' |
| FEN | <u></u> | • | | | | • | 132,69 136,89 136,88 152,88 | 136,89 122,88 136,88 136,88 | | | 135,68 137,68 | 4 | | = | | _ | | - | | a e | | = | 55 | 8 |
| 4 | 88 128.18 138.88 (28.88 126.88 | .00 127,80 118,56 125,09 125,90 | 135,88 135,88 | 132.88 | 88 141,88 141,28 139,88 139,88 | | | | 133,20 133,38 | 7.2 | 3 | | | | . 5 | . BR 149, 88 135, 68 149, cg 158, 28 | NE 128,44 128,88 126,48 127,68 | 115,50 122,80 123,88 | 7 | 127,46 119,98 125,08 126,18 126,88 118,58 125,88 125,98 | .BE 128.BE 120.GR 127.BE 127.BE | 7 | . FF 126.88 117.88 121.88 123.58 | 136 |
| | 7 | 3 | 7 | 3 | = | - | | 72 | = | = | 7 | 7 | 7 | 3 | 3 | = | 3 | 3 | 3 | 77 | 3 | - | = | |
| ¥93 | | = | | 135,68 | | | | | . 2 | 138,88 | | | 3 | | | .3 | 3 | 3 | | | | | | 130,26 |
| ŀ | 2 | 12 | | 7 | 133 | 7 | 2 | 38 | | 132 | 4 | 3 | 2 | 7 | 3 | 7 | 2 | 122 | 75 | 2 2 | 22 | 2 | ě. | 2 |
| Cien | 5 | 40 | == | 2 | 2 | 9 | 6 | 2 | 7 | | | | = | = | | 8 | * | 8 | 9 | 묫릙 | 5 | | = | 133,96 |
| ü | 3 | = | 20,00 | 2 | = | 38. | 56 | 9 | 2 | 139,68 | | \$ | 28 | | | 3 | | 9 | 128 | 25 | | .9 | | 2 |
| COH | | 9 | 133,68 135,58 135,68 .ne 132,68 134,88 | | | , 5 | 139, 48 138, 88 126, 58 | | 133,18 133,38 | • | - 1 | | | = | | = | = | <u></u> | | 2 2 | 3 | = | • | |
| 9 | | 7 | 5.2 | | | 0. | | | 2 | 138,88 | 137.88 | | | .7 | 3 | 2 | | 123.5F | | | .] | | 9 | |
| - | | | | - | - | - | | 126, no 117, 88 | 54 | | | 7 | 7 | 9 | 3 | 7 | = | 3 | 7 | = = = | 7 | - | 7 | .86 131 .86 |
| CS | | | | . = | 5 | | | | 128,88 | 136.88 | 135.88 | | | 3 | 1 | .= | | 7 | 2 | | . 4 | | • | |
| | ĺ | - [| | | | Š | n | 12 | 12 | | | 2 | 21 | ă | ä | - 1 | - [| | - | - 1 | | | | |
| ¥ | 2 | | 20 | | 98 | 66 | 8 | 8 | 2 | 2 | 9 | | | 2 | | | | | 9 | | = | 2 | 8 | |
| | | | 136,88 [36,28 135,16 131,98 ,88 ,88 | | | 122 | 60 123 60 1 | 121,58 | 126,89 | 129,88 | 128 | • | 6 | 123 | | 1 | | - | Ĭ | | -] | | | |
| C2# | = | 8 | 2 2 | = | | 200 | | 300 | 20 | | 92 | 8 | | 8 | 8 | 2 | 2 | | = | = 8 | 2 | | 2 | 5 |
| ٦ | 127.88 127.18 | OF 128, 20 | 36. | 133 28 :33 EE | 133,00 140,00 | 25, | 127,60 | 132,58 | • | • | 1 | 129,38 122,88 | 1 | 2 | 1 | 157,58 135,88 | 128.88 128.28 | .1 | 115,66 129,18 | 110.68 115.86 121.58 | 120,00 121,00 | 115,52 119.00 | 116.98 | :31 |
| .= | | | , - | 8 | | 10 | 200 | | | | 5 | - | - | 2 | | - | | | | | | | 5 I | 80 |
| ÇĬŔ | | • 1 | . 2 | | | 2 | 123,88 | | 127.88 | 126.68 | 127.89 | -0 | 123,06 | | 125.88 | 7.5 | 3 | 118.PR | 2 | 115.86 | | | • | 129,88 |
| | ٩ | - [| 77 | 7 | -7 | . 5 | 2 | | 12 | 12 | 7 | 2 | | ٦ | 2 | 5 | 2 | -= | F | == | 2 | ٦ | | 2 |
| E. | ᆟ | 2 | 4 5 | 5 | 뉙 | • | | 10 | = | 22 | 5 | 7 | = | 2 | ä | 9 | 24 | = | 부 | 55 | • | = | | 15 |
| | 2 | 808611 12 | 20.00 | 2 | | 5 | | 2 | | 201 | _ | ** | - | | | - 1 | او | - 1 | - [| 2 9 | = | | · # . | Ŋ |
| DATE | 866523 | 98 | 888586 888519 | 369522 | 65882 | 888438 | 268581 AAA&14 | 666913 | 000428 | 688428 | 100 | 888428 | 888428 | 606426 | 688428 | 898686 | 898686 | 88618 | 399686 | 586589 867616 | DEB684 | See699 | 119822 | 81584B |
| - 1 | i | - 1 | | - 1 | - 1 | | | İ | | | 6 | 5 | = | 4 | - | - 1 | - 1 | ſ | - 1 | 1 | ı | = | | |
| 310 | 5814 | 2814 | 2888 | 27.62 | 1616 | 3813 | 4785 | 6784 | 1912 | 1812 | 4786 | 1012 | 1811 | 181 | 1811 | 5828 | 5619 | 2915 | 5819 | | 5826 | 181 | 3813 | 2086 |
| HISSION | <u> </u> | ~ | 7 | 7 | 7 | ñ | 46 | 0 | - | = : | 4 | = | = | 7 | ٦ | ñ | ξ. | ~ | ñ | == | 'n | ٦ | ñ | 8 |
| H | 17 | ** | 2 | 1 | 2, | 22 | | l | 23 | 2.4 | | 22 | 22 | 28 | 52 | 5 | 8.4 | 99 | 7 | | 9 | | | 93 |
| • | ~ | ~ i | ** | ١ | N | ₩ | | l. | M | 1 | 1 | N | ** | ~ | N | - | • | - | • | | - | • | | 9 |

TABLE B-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

| - | CZ3A | = | = | 8 | = | 7.20 | 2.5 | 8 | | 2,36 | 3.20 | | 4.68 | 6,78 | 4.38 | 2,66 | 3,0 | 99. | 28 | 8 | = | | === | | = | = | 3,68 |
|-----------------|-----------|-------------|-------------|-----------|------------|-------------|------------------|-------------|------------|------------------|-------------|--------|-------------|-------------|------------|------------|-------------|-------------|-------------------------|------------|---------|-----------|---------------|--------|------------|-----------|---------------|
| | C22A | 1.56 | 53 | = | 8 | . 5.5 | 1.00 | 2.28 | = | .66 | 1.88 | ; | 1.48 | 2,68 | 5.88 | | 72. | .23 | 8 4 | 7 | . 5 | | 3.5 | | | | 1.0 |
| | C214 B4H | 1.59 140.99 | 1.20 142,10 | .48 | .41 134.6E | 1.18.142.49 | 1.68 145.16 | | .68 135.28 | | . 83 142.88 | 371 | 4 | 2,80 149,28 | .58 136.88 | .73 149,18 | .66 144,38 | 1.18 | 5.29 168,48 5.98 .88 | 58 135,69 | .32 .00 | 50 134.30 | 1 | | - 41 | 135. | .00 139,90 |
| | C284 E1H | 1.39 142.70 | 1,18 | 47 /48,88 | .44 137.28 | 1.69 | 78 145,48 | 2,88 154,88 | . 52 | 2.68 .88 | 10. 10. | | 1.00 149.68 | 1,78 152,48 | .58 141.88 | .65 145,00 | . 83 149,88 | 3,78 126,00 | 9,46 177,28 | .55 142.48 | 137 166 | 54 142.18 | 98 481 47 | 3 | 149 137,18 | 49 136,00 | .70 |
| | Z84 | 1,45 | 4.18 | 2.58 | 1,86 | 3.38 | 200 | 6.38 | 1.98 | 2,18 1.78 | 2.88 | 2.58 | 7.00 | 5,38 | 1.48 | 1.58 | 2,00 | .2.88 | 20 7 | 11 | 2, | . 83 | .76 | 27. | .76 | 27. | 3.56 |
| | 844 | 1.65 | 5.36 | 2.38 | | _ • | 5.28 | 7.88 | 3,68 | 2.08 | 4.25 | . C. | 6,28 | 7.86 | 2.66 | 3,38 | 2,88 | 1.78 | 229,65 | 2.10 | 22 | 2.3F | 1.18 | 2,00 | .22 | | |
| | C244 | | 2.18 | 1:48 | . 88 | 2,28 | 2,28 | 3.66 | 1.28 | 1,00 | 1.40 | 1,68 | 1.78 | 2.86 | .68 | =, | 1.8 | 3.8 | 5,38 2 | 1.86 | . 82 | 1,98 | 1.00 | 96. | . 8.8 | .78 | 1.68 |
| | Ciga | - | 1,48 | . 48 | .37 | 1,48 | 8,5 | 2,60 | . 90 | 1,28 | 1,05 | 1,58 | 1.38 | 2,10 | .56 | | 1.00 | 1.45 | 15, 88 | . 62 | ,27 | 99. | 45 | 89, | . 33 | n | |
| | C111 | 1.23 | 1.44 | 8 | 1 | 1,48 | 1,88 | 2.68 | | 2 S | . 56 | | 1.78 | = | .48 | 1.80 | 1.96 | 200 | 14.78 | 56 | .33 | 99 | 4. | *9 | • | .48 | 6, |
| | £174 | . es | 2.18 | .67 | 36 | . • | 12.7 | 3.86 | 1.38 | 1,00 | 1.40 | 2.28 | 2.86 | 3,88 | . 68 | 1.68 | 1.38 | .57 | 38.58 | 86 | 57 | 200 | . 48 | | | .37 | 1.28 |
| | BEC | Ä | | 2. | i.s | = | = :: | 4 | | 5 64 | ī | 23 | = | 22 | 11 | 23 | 29 | ~ | 7.5 | 22 | = | = | 21, 21 | = | - = | . 11 | 2 |
| 12041 | DATE | SBR623 | 616919 | 988523 | CERGIT | E. | 688519 688527 | 868519 | - | 8F#5#1 868917 | 856428 | 513428 | 826361 | 856428 | 888428 | 866428 | 868425 | 856918 | 898618 | 689586 | 688618 | | 898616 | 687686 | 880669 | | C88513 |
| SHITCH POSITION | HY SISTEM | 1818 | 1916 | 5814 | 3914 | 2862 | 2782 | 1816 | 3013 | 3784 | 1812 | 1812 | | 1012 | 1811 | 11811 | 1011 | 4823 | 5828 2815 | 5819 | 2815 | 58.7 | 1613 | 5826 | 1811 | 3813 | 2886 |
| 211 | 15 | • | • | 12 | •0 | 0, | | 12 | 22 | | × | 24 | | 22 | 27 | 28 | 58 | 57 | 5 | 78 | 98 | 83 | | = | *** | | 8 |

CONTRACTOR OF THE PROPERTY OF THE PARTY OF T

TABLE B-1 (Continued)
OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT
CONDITIONS LISTED IN TABLE 3

| ! | 120 | | 2 | 8 | | 2.5 | 2 | 1 | 7. | 1.10 | 1.48 | | | | 1 | | : | = | 1. | : | = | = | • | 1.5 | 3 |
|------------------|--------------|--------|--------|----------------|--------|------------|--------|--------|--------|------------|--------|--------|----------|--------|--------|--------|--------|--------|--------|-------|------------------|--------|-------------|------------------|--------|
| i | D\$ 4 | .13 | 412 | # | 7 | 2.5 | 20 | | == | 27. | 2.3 | : | 7 | : | 2 | 2 : | | = | -12 | .12 | 2: | == | = | 25. | = |
| | D134 | -12 | 919 | = | | 3.5 | 87 | 5 | 21. | 51. | 25 | 3 5 | 2 | : | 3.3 | 5 | | 1:0 | = | 97. | =: | = | = | | 97 |
| - | 790 | 3 | 121 | .15 | 4.0 | 7,6 | .5 | . 27 | -24 | 'n. | 86 | | 72. | | -27 | 2 5 | | 5.50 | === | 71. | 12. | = | .28 | 22. | .30 |
| | D184 | | | | .10 | === | | | 69 | G 1 | 21, | 1 | | | =: | | | 1.28 | = | .10 | a ; | = | | ## | 91; |
| * | D2A | 36. | ,28 | 315 | .58 | 138 | 7.5 | .32 | er: | .42 | 88. | | 38. | | 5 | 32 | 3.76 | 4,28 | 110 | 2 | 12. | 1 | .28 | 2.5 | 141 |
| | D114 | | 2,01 | = | . 58 | 2.18 | 2,41 | .32 | .38 | .48 | 7.5 | 2 | . 28 | • | 38 | | . 97 | .75 | 56 | 3 | 25. | | | 95° | 25 |
| | D16A | S) | 21 | | . 36 | •28 •26 | -8- | .18 | -17 | .25 | 3,5 | 8 | . | 60 | 81. | . 22 | 3,58 | 4.48 | .12 | = | 4: | .11 | = | 2.5 | .20 |
| į | D7.A | = | | 91. | • | | 12. | .16 | 11. | 11. | 7.3 | = | | | 2: | . 88 | 7 | 1.10 | = | = | = # | = | 9. | 2.2 | • |
| | D8A | 91, | | 112 | 121 | | , 26 | 116 | :13 | 51. | 2.7 | | se' | | f 16 | | • | 1.00 | ¥. | :12 | 715 | -12 | 2 7. | 2,2 | 92, |
| | D54 | \$ | . 16 | . 28 | 50 | . 5 | 99 | .33 | 38 | .45 | 9.9 | 88 | .36 | • | 18. | 45 | 2,65 | | | .12 | 2.5 | 92° | 13. | N.P | 37 |
| | 770 | N. | 112 | - | | ¥.£ | . 78 | . 25 | -28 | , 48 | 4.5 | 98 | = | | 10 E | = | 2,95 | 99. | .16 | | | 8 | .18 | ÷: | 38 |
| • | REC | 8 | is | 7. | 2 | 222 | ī | • | 41 | 12 | 2.5 | 36 | 12 | 24 | 25 | 7 | 15 | 17 | 34 | 12 | 2,0 | 23 | = | 22 | 9 |
| 10H2 5 | DATE | 899623 | 686523 | 55861 <u>1</u> | 368586 | 886519 | 888519 | 866438 | 888551 | 866428 | 566428 | 866428 | 888428 | 846428 | 888428 | 686428 | 888689 | 869518 | 989868 | 81968 | 588685 868683 | 919989 | 909089 | 868689 886611 | 966515 |
| SHITCH POSITION: | HTSSION | 1816 | 5614 | 3814 | | 1215 | 1916 | 3013 | | 1812 | 1912 | | 1015 | | 1011 | 1 1 | 1016 | | SEIS | | 5818 | 1 | 5828 | 1811 | 2886 |
| SHITC | 2 | ٠. | 12 | | 19 | | 22 | 22 | | 23 | 77 | 23 | 27 | 28 | | 29 | 99 | | 3 | 9 | 8 3 | | 5 0 | 8 | 36 |

or the state of th

TABLE B-1 (Continued)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLICHT CONDITIONS LISTED IN TABLE 3

| 1484 | = | 4 | = | • | | | 1 | 2.00 | 4,26 | 9.86 | 7.00 | 18.5 | 97.5 | | | 6.06 | = | 4 5 | : | | | 1 1 | | = | 5.5 |
|-----------------|----------|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|---------------------------------------|--------|------------|--------|------|-------|--------|--------|
| 777 | 4 | 99 | 52 | | 2 | 2.66 | | 25.7 | 2,18 | 3.10 | 100 | 4418 | 7 | 1.70 | 1.1 | 2.28 | 23,28 | 21.41 | · | : | 26. | 7 | 1 | Į. | = |
| £284 | 1.27 | 1.66 | | | | | | 2.5 | 3,86 | 4.18 | = 7 | 5.28 | 1.50 | 9.15 | ř. | 20.5 | 124,16 | l l | • | | 1.0 | | | | 2,06 |
| 1924 | 14 | 7 | | | | | | 35 | 19. | .63 | | . 86 | 52 | | r. | .42 | | | | | 5 | | | 22. | .5 |
| C264 | .5 | | | | | | • | 2,28 | 3,86 | 4,20 | 17.7 | 9.10 | 1,78 | 2.34 | .28 | 3,66 | | ֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓ | = | | | | | = | = |
| 4154 | 742 | . 26 | .23 | | = 1 | 26 | | 17. | 5 | 99. | | | 2,50 | 98. | 7. | 55 | 2,06 | | .5 | | 22. | | | 2. | = |
| 1997 | 299 | 1.46 | .38 | | 50,0 | | | 20.0 | 4.0 | 5.66 | 989 | 2,38 | 4.20 | | | 5.80 | 16,40 | | | 88 | 57. | | | | 3.56 |
| 4454 | .92 | | -42 | | 8 | | | | 1,46 | 2.18 | 2.58 | 3.90 | 1 | 17.16 | 1.66 | 2.10 | 11,20 | | 52. | 67 | # C | | | 42 | 1:10 |
| 2227 | iii | 1.50 | .70 | • | 2,00 | | | 7.00 | 9.36 | 14.00 | 15.66 | 13,68 | 92.9 | 7.36 | 7,88 | 6.11 | 115.10 | 30.6 | | 1.78 | 99 | | | | 5.18 |
| 4564 | u. | . 35 | | | 85. | 1 | | 7 | 3. | 7.78 | | 1,10 | 128 | .37 | BC. | 99. | 2,08 | | 22. | 8 5 | 98, | | * | F. | 39 |
| V65V | 55 | . 30 | 3 | | 3. | | | , | 45 | 39. | | .95 | .27 | 85 | .26 | 38. | 2,58 | 28 | 717 | 9 7 | ,27 | | ě | 22. | 38. |
| 525A | = | 1.16 | .49 | | 2,48 | 9 | | 1.6 | 2.58 | 3,78 | 4.39 | 4.85 | 1,48 | 2,68 | 1.48 | 2.78 | 2.28 | • | 9 | 1,68 | 38 | | : | 5 | 2.68 |
| Ä | | 2 | ,5 | | 2: | 2 .3 | | = | 13 | 25 | 7 | 37 | - Si | | 59 | 7 | 2: | ¥ \$ | 2 | ņ | 5) | .0 | ,, | 22 | 5. |
| 1 1 | 2598622 | 618523 | 366611 | 888586 | 882519 | 846519 | 066430 | 105009 | 111428 | 886428 | 683561 | 864428 | 88428 | 888428 | 888428 | 186428 | 689888 | 966686 | 996614 | 855686 | 009699 | 2000 | 98489 | 119988 | 815889 |
| TE MISSION CATE | 1818 888 | 5914 662 | 3014 | | 1815 | 1 1 | | 4785 | 1012 | 1012 | - 1 | 1612 | 191 | 1181 | | 161 | 1819 | i | 1 | | 3707 | i i | | 3013 | 2886 |
| 7 | | 17 | 20 | 5 | | Zi | 22 | | 23 | 3.6 | | X | 22 | 25 | | 29 | 29 | 3 | 98 | 13 | | 2 | = | | |

TABLE 8-1 (Concluded)

OVERALL RMS LEVELS PRODUCED BY STABILIZED FLIGHT CONDITIONS LISTED IN TABLE 3

| 1 | A12H | = | = | 3 | 11-11 | 2.2 | = | 148,10 | 143,10 | 145.86 | 138.00 | 18.0 | 135.88 | 131,00 | 132,00 | 3. | = | = | 2: | | • | | 15 141.98 |
|------------------|-----------|------------|--------|--------|--------|------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|----------------|--------|--------|----------------|-----------|
| | 2210 | 8 | = | 4 | 28 | 2:5 | | = | 2. | 2 5 | 191 | | | 191. | .121 | 35. | = | = | =: | = | • | 11. | 315 |
| | £151 | 27.00 | 15.81 | 23,86 | 28.38 | 26.59 | | 3, | 19,08 | 3 2 | 19.39 | 20.25 | 18.89 | 29.93 | | 29,28 | 19,38 | 23,86 | 27.00 | 27.00 | 24,29 | 23,66 | 28.28 |
| | 1913 | 20,00 | 11.00 | 16,00 | 28.28 | 19.46 | 70. | • | 19.68 | 17.28 | 10,00 | 19.10 | 16.00 | 16.28 | 26.88 | 21.10 | 17.00 | 18.88 | 21.55 | 29.78 | 20.08 | 22, 68 | 19,30 |
| | 19 | 1.56 | 1.28 | 1.58 | 1,18 | 1,12 | 59. | .7 | 7. | 5.5 | 1.58 | | 7. | 3. | ¥. | 2,38 | 1.28 | 2. | =: | = | .72 | 8.5 | 1.48 |
| | 1341 | 17.48 | 17,00 | 15,00 | | 19,01 | | = | 14,18 | 27. | 15,38 | 15,38 | 15.44 | 15,38 | 15,20 | 19,00 | 15.18 | Ξ. | 2.0 | 2.00 | 17,90 | | 17,00 |
| | £134 | 15,30 | 26.98 | 7,68 | 37,16 | 36,48 | 25,30 | 25,00 | 35.98 | 23.86 | 59,58 | 23,06 | 14.86 | 33.70 | 27.06 | 97.9 | 2°. | 2.5 | 8 | 1.20 | 7.98 | 7, 88 6, 58 | 36,38 |
| | £13.4 | 37.80 | 31.06 | 28,86 | 47.66 | 24,00 24,00 | | • | 45,38 | 5.5 | 65,08 | 32,68 | 33.60 | 38,10 | 51.86 | 38.08 | 26.29 | 29.80 | 36,36 | 32.90 | 34.8 | 37.18 | 35.00 |
| | 112 | 35,64 | 29,86 | 25, 86 | 42,00 | 88 88 88 88 | | • | 35.38 | 38,88 | 38, 66 | 22.58 | 28.88 | 27,38 | 41.11 | 36.38 | 24,18 | 26,88 | 24,52 | 22.78 | 29,28 | 26,00 | 36.49 |
| | £\$1 | 796 25, 68 | 25,88 | 28,38 | 29, 69 | 28, 88 | | | 27.08 | 36,28 | 38,68 | 24,58 | 28.00 | 25,48 | 27.00 | 36.88 | 18.48 | 21.H | 20,52 | 15, 86 | 10.00 | 2 3 // | 35,60 |
| | ā | | 22,38 | 18.66 | 33.28 | 36,88 | | 5, 11 | 11,38 | 11 | 15,66 | 16,49 | 18.88 | 12,00 | 38,88 | 28,78 | 18,8 | 22,28 | 17,8 | 28,88 | 18.06 | 16.00 | 26.08 |
| | 123 | 85.98 | 116,98 | 58,26 | 85,26 | 73,28 | | 2 | 64.48 | 71.E | 86,88 | 42.78 | 41.00 | 47.18 | 54,28 | 108.00 | 77.9 | 81.58 | 58,00 49,00 | 45.78 | 45.60 | 51.50 64.10 | 58.68 |
| = | 1 | 2 | .E. | 16 | 7 | == | 100 | 21 | 2 | 2 2 | 2 | 4 | , in | 28 | 7 | 2 | 93 | 2 | 23 | 2. | 5 | 2.4 | 뉙 |
| - 1 | DATE | 899623 | 196523 | 119061 | 898556 | 868519 668527 | 357983 | 366561 | 888428 | 806428 | 669428 | 868428 | 800428 | 898428 | 838428 | 888689 | 2000 | 916919 | 325258 | 919019 | 989888 | 888689 | 846513 |
| SHITCH POSITIONS | HT\$\$10H | 1810 | 5914 | 3814 | 2888 | 1615 2782 | 3813 | 4785 | 1912 | 1912 | 1012 | 1811 | ł | 1101 | 1251 | | 2619 | 2115 | 6186 | 101 | 3628 | 1811 3815 | 2986 |
| SATT | 3 | • | 2 | = | : | | 122 | | F | 72 | 22 | 2 | | 28 | 23 | 3 | 7 | 5 | 48 | | = | • | 3.6 |

TABLE B-2

のでは、1000のでは

| | | | | PEAK OR MAXIMUM RMS LEVELS PRODUCED BY TRANSIENT FLIGHT CONDITIONS LISTED IN TABLE A | MAXIM | M RMS | LEVELS STED 11 | PRODU | CED BY | TRANSI | EX |
|-----|------------------|-------------------|------------|---|-------|------------|-------------------|-------|-------------|-------------|------|
| Sul | SWITCH POSITIONS | TYONE | - | | | | ; } | | ا | | |
| ų. | TC HTSSION | DATE | PEC | 414 | 424 | B1A | A29A | 1821 | A42A | 111 | 7817 |
| - | 3812 | 10145 | • | 7 | .20 | 7 | 24 | 8 | 2,48 | 2,48 115,20 | 2 |
| | 67.82 | | 1. | | | \ | | | 2 | 120-021 | Z: |
| | 6784 | 68913 | • | 16 | 2.5 | 722 | 36 | 110 | 7 S | 35 168,86 | |
| ~ | 1916 | 608519 32 | 2 | . 38 | 38 | 181 | 89 | .33 | 1.29 | 1,29 110,00 | . 5 |
| • | 1811 | 1811 688428 | ~ | 35 | 25 | 21, | 28 | | 1.48 133.98 | 133,90 | |
| m | | 1812 888428 42 | 12 | .34 | 38, | .48 | .57 | .24 | 1.34 | 1.36 126,48 | |
| | 5819 | \$5555 \$5555 | S N | 5.41 | \$3. | 96. 96. | 3, 69, | 3,4 | 1,35 | 35 136,38 | 7,7 |
| 13 | 27.82 | 838527 <u>1</u> 6 | | 2,36 | 12.20 | 1,38 | 2, 86 | | 15.03 | | |
| | 5828 | 5898¥8 7896\$8 | Z % | 2.28 | 81°3 | 27.5 | 22,26 | 2 | 8. | 20.00 | z. |
| | 2013 | 119000 | | ł | 1.16 | 1.27 | 2.13 | ř. | 2.5 | 3,12 131,99 | |
| F | 1812 | 102428 | 3 • | 1.00 | 7.2 | | 2,48 | 3: | 8. | .06 129,16 | R. |

| 193 | 2 | # 2 : | 12.2 | 1 2 | 1 | Ę | 7.3 |
|-------------|-------------|------------------|--------------------|---|------------|-------|---------------|
| 707 | 2 | | 2.5 | | 2.5 | ı | 1.25 |
| 181 | 7. | 77.5 | 3.5 |] : | 4. Y. | | 5 |
| 797 | 25: | 3 - 7 | X, Z | | 22.22 | | Ą |
| 1111 | 7.1 | 2 2 | 7.5 | 25 | r S | .37 | ¥,7 |
| V66V | 17 2 | | 757 | 1, | 2.2 | | 24 |
| 767 | 3.5 | 25.5 | 52 | 59 | 7.5 | 1,37 | 1, 48 . 55 |
| 747 | === | | 3,5 | \$19 | . 5 | 29 | 36 |
| 1461 | 20.5 | 22 | 22 | 2 | 8 S | . SE | 23 |
| A35A | 25 | | 21,13 | 217 | 2 | \$ | ř. |
| 1221 | 21.5 | 3.2 | 2.5 | 21. | : 5 | 2 | 7.4 |
| 4254 | 2. | 12. 24. | 22 | ======================================= | .52 | 27 | 36. |
| REC | | | | 2 | 2 | | 7 7 |
| DATE | \$4643£ | 862586 868523 | \$88527 \$68611 | 136961 | | 11994 | 1623 |
| 473550H | 3013 | 2078 | 3613 | 4785 | | Sign | 78.4 |
| 10 | 1 | | | ~ | | | |

SAITCH POSITIONS

TABLE 8-2 (Continued)

是他们是他们的人,也是不是一个人的人,也是是一个人,也是是一个人,也是是一个人,也是一个人,也是一个人,也是一个人,也是一个人,也是一个人,也是一个人,也是一个人 第一个人,也是一个人,也是一个人,也是是一个人,也是是一个人,也是是一个人,也是一个人,也是一个人,也是一个人,也是一个人,也是一个人,也是一个人,也是一个人,也

PEAK OR MAXIMUM RMS LEVELS PRODUCED BY TRANSIENT FLIGHT CONDITIONS LISTED IN TABLE 4

| | 2 | 3,68 | 3,81 | | | 2 | 2 | = | = | : | = | ŧ | • | 5.10 | | 164 | 1.53 | 1,24 | ===== | 45 | | | | == | = | 55 | 8 | 37.5 | 4.46 |
|-----------------|---------|-----------|--------------|--------|--|--------|--------|------|------------|--------|--------|----------------|-------|--------|-----------------|-------------|----------|--------|-------|--------|-----|---------|--------|--------|-------|------------------|--------|--------|--------|
| | 787 | 36 | 7, | | | 27 | 2.10 | 90-1 | 3 | 52.3 | 25 | .71 | Į | | | 4354 | Ė | 71. | 7. | | | | 35. | 7.5 | ę, | 1 E 3 | 8 | 3 | 100 |
| | 157 | .44 | 3, | | 25 | 27 | 2.8 | 2.48 | 2,36 | 2,15 | 7.07 | 7.7 | 1,28 | 2.39 | | 1961 | ž | S. | 3 | 5 2 | . | | , y, | 3,7 | \$7. | 3 Z | 8 | # | 8 |
| | 797 | .32 | z; | 2 | Ä | 8 | 97 | | 1.36 | 1.28 | 96 | | 8. | 1.40 | | 1341 | Ŧ | 41: | ×. | 5 | | | 34 | ц, | 25. | 2.3 | 8 | .5 | 8 |
| | 1411 | * | 7 : | | 5 | 1.8 | 1.94 | ×.× | 25. | 20,7 | 12. | r. | S. 88 | 2,18 | | 824 | 30,23 | 28,48 | 22.52 | 127.56 | | 145,21 | 40.05 | 141 | 27.30 | 141,8 | 189.46 | 196,79 | 160,20 |
| . | 4394 | . 48 | 5. | | K | 1.78 | 3,48 | 7.98 | 1,36 | 2,94 | 5 | | 2,48 | 5.18 | | 1 24 | 123,90 8 | 9 | , | === | | | | 122,00 | | 22 | 31.00 | 132,96 | |
| 1 ABLE | 191 | 1.64 | 1.62 | | 5 | 7.00 | 9.0 | | | | 3 | ř. | 1.36 | 99.6 | ! | 1441 | 15. | | | 7 24 | | 7 | | 2.5 | = | 2,1 | 3.38 | 2,06 | 3,66 |
| EU 18 | 161 | 449 | 2 | | 19 | 1.63 | 2,48 | 2.78 | = | 1,78 | | 16. | | 2.48 | | 4434 | 23. | 2.5 | ä. | = 2 | | | ř | ñ, | 3 | == | 3 | 5 | 7. |
| 3 | 1461 | 97" | 8 5°, | | 2 | 1.28 | 2,78 | 2.90 | 2. | 2,28 | | 1.28 | 2.96 | 2,68 | | 924 | 2. | 1. | | | , | | 2,56 | 2.0 | 75 | 22 | 33 40 | 10.00 | 51,00 |
| CURDI I IURS | A38A | .39 | ,33 | | 'n | 2,48 | 6.71 | 9,28 | 35 | | | 7.7 | 2.00 | 7.48 | | 134 | ¥. | 2 | 3 | 7 | | , | 95. | 2,5 | 5, | 22 | 7,38 | 3,38 | 8 |
| | 1221 | .34 | 4. | | 5 | 1.00 | 2,06 | = | | 2,00 | 2 | .72 | 1.20 | 1.28 | | 1364 | 3. | 91° | | | , | | ,26 | 2,2 | 13. | 2.2 | 2.46 | 2 | 99.3 |
| | 1221 | . 34 | 7. | 33 | .27 | 1,00 | 2,39 | 2.98 | 1.43 | 1.75 | | | F. 1 | 2.00 | | 43E4 | 11. | 12. | 7 | 27.7 | | | .32 | 5,5 | ŝ. | 2.3 | 1.63 | 2,0 | 1.20 |
| ~ | E. | 2 | 5 : | | ֧֧֓֞֝֝֝֝֝֝֝֡֝֝֡֝֝֡֝֝֡֡֝֝֡֡֝֡֝֡֡֝֡֝֡֝֡֡֡֝֡֡֡֝֡֡֡֝֡֡֡֝֡֡֡֡ | • | = | iri | 122 124 | 9 5 | 2 | 4 | = | • | 1 | J. | - | 7 | 22 | ** | | N (| ~ | 5 % | 2 | 22 | 12, | 2 | 4 |
| 1041 | DATE | | 110428 | 767900 | 689988 | 889527 | 880519 | ñ | 989688 | 198527 | 989888 | 2000 11 | 98638 | 215000 | 100 | DATE | 068428 | 888428 | | 25500 | | \$86525 | /25981 | 200519 | 11999 | 100510 100664 | 161434 | 196999 | 864513 |
| SHITCH POSITION | E155104 | | | 1 | | - 1 | 1816 | | 5819 | 2742 | | | 3412 | 2886 | SAITEN POSITION | H18810H | 1101 | | 1 | 2886 | - 1 | 7196 | | 1616 | | 1813 2819 | 5612 | 2945 | 2886 |
| SXITC | 2 | tn | | | | • | 12 | 14 | | 51. | | | 9 | 6 | 34170 | T H | - | 2 | | | , | • | | 5 | | 2 | 22 | = | 2 |

TABLE B-2 (Continued)

PEAK OR MAXIMUM RMS LEVELS PRODUCED BY TRANSIENT FLIGHT COMDITIONS LISTED IN TABLE 4

| | EBA | = | 2 | 1 | | | = | = | == | | 2.16 | | | | 6.42 | 72-72 | | 87. | 33,88 | 51,48 | 4: | 37.52 | 22: | |
|------------|---------|------------|-------|--------|--------------|----------|-------|--------|----------|------------|-------|--------|-------------------------------------|-------------------|----------|-------|--------|-----------------|---------------|--------|----------|------------------|----------------------------------|---------|
| | 1111 | 12. | =; | 1 | 2 | 2 | 877 | 2,40 | e 8 | | • | | | ; 3 | - 1 | 1 | 3 | 37. | - 1 | 2.8 | 2.12 | E.S | 1 1 | 4 |
| | 1821 | 2. | z: | | 2 | * | 7 | 7 | 27. | ķ | Z, | 417 | 1616 | | 2,1 | 1 | 7. | 77 | į | 7,3 | = | == | 72: | ş |
| | 4144 | 17. | =: | 7 | Z. | 2 | 77 | .74 | 22, | 3 5 | 2 | 213 | 163 | 21.06 | 2, | | 2.7 | 117.18 77.88 | 3. | 115.50 | 2.2 | 26.50 | 2 2 2 2 | |
| | 4194 | z. | ă. | 1 | = | | 25 | 3,16 | i E | 2.88 | 1.0 | * | | - | R: | : | | | s. | | • | 6.9 | | 1 1 |
| | A133 | == | | | Ą | | 200 | 5,38 | - E | 7 | 2.96 | | 615 A | | 2 5 | 3 | R. | N.F. | | ĄX | = | ₹.5 | 252 | |
| ABLE 4 | 4104 | .14 | 7.3 | 1.20 | 1,20 | | 200 | 85.82 | 7.5 | 5.7 | 4.88 | . 32 | E124 | 1.18 | 30,86 | 3 | 2. | | 44,48 | 33.90 | 2. | 38 | 22.52 | 33, 00 |
| K | 7617 | 71. | 17. | .32 | . 30 | 1 | 7.88 | | | 2,98 | 1.50 | . 42 | D144 | 27. | 10, | ı | ı | 23. | 98. | 36 | | 2,2 | 527 | 1 |
| LISIED | 4334 | SB. | 3.5 | 3 | 20. | 1 | 2 | 95 | 1 | 227 | 12. | 71 | 15E | 9.78 | 136,86 | 3 | 7,00 | 7.7 | 3.86 | 143,06 | 20.5 | r z | 139,26 | 80.0 |
| COMPLITORS | A37A | 8, | 2 2 | | 1 | | 2.2 | 3 | 2,2 | 4.5 | 2,48 | .34 | 3 | .91 117,40 129,78 | 21 69 62 | | | 131.90 13 | 142,86 143,00 | | 2 | 2,3 | . 90 13 125, 96 14 124, 96 | |
| | 4124 | 9 . | 7, F | 36 | 1. | • | 7.5 | - | 7.4 | 7,18 | 7.61 | .71 | 19 | 11 16. | 1,42 13 | | de e | 27 27 17 | 6,00 14 | 35. | 7.28 127 | E : | 4,20 12 | 6,36 14 |
| | 4114 | 91. | == | 38. | 91. | | 2.73 | | 2,36 | 2,28 | 1:00 | | 7 | 9. | 2.5 | | | 2.73 | 5.78 | 7.65 | | 7.46 | 3,56 3,26 | |
| • | nec. | - | 25 | | 8 4 (| | 2 | 1 | ** | 21 | 12 | | 3 | - | a n | | Ì | | | 20 | | ~ • | 19 22 26 | |
| | BATE | 900611 | 92750 | 166430 | 348519 | | 22.04 | 100523 | 196628 | \$50439 | 90000 | 119000 | | 95999 | 196901 | 200 | 800513 | 00013 | 105000 | 100564 | 10000 | 940913 140913 | 000518 600609 000611 | 106430 |
| POSITIONS | HTSSICK | 2017 | 1811 | 1 1 | 1813 | 1 | 21/2 | | 5812 | 2012 | 2882 | 3014 | SWITCH POSITIONS TC RESSION DATE | 2015 | 47 85 | i | 2906 | ł | 4766 | 2000 | ł | 6762 6 | 1015 1011 3013 | 3012 |
| SWITCH | Te HI | - | ~ | • | | ! | 77 | 77 | | 21 | = | 2 | SMITCH TC RT | - | • | | | | ŀ | = | | £3 | 91 | 22 |

TABLE B-2 (Continued)

PEAK OR MAXIMUM RMS LEVELS PRODUCED BY TRANSIENT FLIGHT CONDITIONS LISTED IN TABLE 4

SMITCH POSITIONS

| 1210 | S. | | 7 | 1 | 2 | | 1.73 | ž | 3. | 3. | 32.96 | 8. | | H | | £134 | 2 | 1 | | 7 | 3 | 4 | | 2 | 2 | 1 | 1 | | 51.18 |
|---------|------------|---|-------------|--------|--------|----------|--------|--------|-----------|----------|--------|--------|-------|--------|------------------|-------------|--------|--------|--------|-----------|---|---------------------|--------|-----------|----------|---------|--------|---------|-----------|
| 1210 | 22.23 | | 37-171 98-6 | 69-69 | 148.38 | | 127.28 | 150,00 | 136.46 | 145.00 | 136,86 | 128.06 | 27.78 | 134,66 | | 4113 | = | 3 | | 3. | 2 | 9 | | 20.0 | 2. | | | | 2 |
| 763 | 7,5 | 1 | 20.00 | | | | 36.50 | | 14,99 | 24,00 | 22,96 | 23.01 | | 11.66 | | 1219 | = | 3 | 5.9 | 7, | 2 | 8.8 | 1 | | 31.20 | | 11.18 | 7.60 | 51.0 |
| 7018 | 2.2 | | | 96-9 | 5 | | 9 | .83 | 14.48 | 90.0 | 9.6 | 3. | 3.61 | 2.00 | | 1919 | 7. | 8 | 7,48 | S, | 3 | 19.00 | • | 3 | 8.3 | 26.34 | 26.20 | 77 | 63.68 |
| | 27,22 | | 152.86 | 153.90 | 149,46 | | 140.00 | ŗ | 164,96 | 160,00 | 196,88 | 152.90 | 36.18 | | | ¥. | 121,8 | 121,00 | 133,00 | 126.71 | | 44.8 | 116,65 | 143.60 | 143.99 | 8 | 152.68 | | Ę |
| | 126,00 | | 134.00 | 2 | 136.00 | | | | 149,48 | 156,86 | 144,88 | 132,84 | | 136.00 | | 5514 | 131.86 | | 닠 | | | 23.48 162.69 144.00 | 163,00 | 2 | 175,58 | 165,00 | | 177.69 | 177.68 |
| 27118 | z,z | | | | 뉤 | | d | Ŗ | 19.40 | 8. | 18.00 | 2: | | • | | E124 | 3,06 | 1,10 | - 1 | 7.5 | | 23.41 | 16.00 | 6.78 | 36.18 | 5,00 | 15.20 | 34.36 | 36.10 |
| 17119 | 2,52 | | 3.84 | 2,76 | 3.27 | | | 71. | 6.78 | 20.50 | 3.28 | 3: | | | | 163 | 110.66 | 126.06 | 25.45 | 120,18 | | Ziveli | | | 136.00 | 135, 86 | | - { | |
| 14 | 95 ° 7 | | 2.59 | 2,2 | 2.42 | • | 6.23 | | 6.78 | 8,78 | 13.28 | N . | | 20 | | 8134 | = | 38. | | | | Zall 12Pall | 4.88.1 | 3,40 | 1 84 97 | 1,70 | | 23,00 1 | 36.18 1 |
| | X (| | 27.7 | 2 | 2 | | | 2 | 16,18 | 5.48 | 8.78 | 2 . | | 2.0 | | 9144 | 23. | 26 | 27 | | | | 17.7 | 2,28 | 121,48 | 20.5 | - 1 | 5.78 | |
| | 127,86 | | 134.38 | 276,00 | | | 100 | 127,58 | 144,50 | 147.58 | 3. | 20.95 | (| 2 | | B14H | = | 118,06 | | 124-86 | | | 143.00 | 12°86 | 1 96 391 | * | | 146,14 | 145,65 |
| B7.H | 133,18 5 | | 156.22 | | 157.48 | . 25 50 | | | 1 44,96 1 | 147.50 1 | 156,06 | 136,26 | | | | B134 | 114,00 | | 11.62 | 123,00 13 | | | | 128.88 13 | 155.28 1 | 123,06 | 7 | | 142,98 17 |
| 2 | #20 84 | | 4 | | 1 | | ł | Z N | Z | 22 | 21 | 22 % | i | = | | ž | - | 2 | 1 | | [| 1 | j | 7 | 77 | 56 | J | | <u> </u> |
| .] | 119901 | , | 14504 | 2007 | 11653 | Panera . | | | 615000 | 119969 | 105901 | 300519 | | 404615 | | DATE | 015000 | 888618 | 22001 | 816913 | | | 996391 | 588623 | 888519 | 119860 | 11011 | 301395 | |
| MISSION | | | 47.00 | | 1816 | | | | 9161 | 3613 | 4705 | 1815 | ţ . | 2014 | SKITCH POSITION! | H12510K | 1915 | 1 | 1 | 22.6 | 1 | 1 | - } | 1616 | ' | 5105 | 1 | 4785 | |
| 2 | - | | 4 | | | | | İ | - | 12 | 3.4 | 31 | | 2 | SKITC | TC M | - | ~ | | | , | | 40 | | • | 12 | | = | |

TABLE B-2 (Continued)

.

1、文書の「大学のでは、いる人の相手に関いている。」というでは、他们は「大学のでは、大学のでは、大学のでは、大学のでは、「大学のでは、大学のでは、「大学のでは、「大学のでは、「大学のでは、「大学ので

PEAK OR MAXIMEM RMS LEVELS PRODUCED BY TRANSIENT FLIGHT CONDITIONS LISTED IN TABLE 4

| | £134 | 58,86 | 42.81 | | 22,91 | 21.75 | 3 | 8. | CITH | 1 | 2 | • | 10.75 | = | 5. | 2 | Į | = | Ą | 3 | 167.18 | 3. | 98 | 3 | | | Ж | 165.2 | | • | | 1 | į | 3 | = | Ę | 3 | | |
|------------|---------|----------|-------|-------|--------|------------|--------|---------------------------|------------|------------|--------|--------|--------|--------|--------|-------|--------|-------|--------|--------|--------|--------|--------|--------|-------|--------|---------|---------|---------|----|---------|-------------------|--------|--------|--------|--------|--------|--------|---|
| - 10 | EIIA | 5,46 | | 5.00 | 3,34 | 7-7 | 5 | 9,38 | C1 B4 | 115,60 | 2 | 2 | 57.36 | _ | 63.66 | 26.98 | | 58-31 | Į | 163.28 | 163.36 | 161,04 | 164,98 | 162,64 | | 2 2 | 22.5 | 2 | 1 | | | 155. | 37.5 | 143,00 | 52.00 | | 2 | 152.60 | ł |
| į | 1210 | 6.23 | 1 | 9.24 | 9.30 | | 8.00 | 10,29 | £24 | • | 167.86 | = | | | | | | | 164.14 | | | | 1 | 2 | - 1 | | 9 | 62.21 | 1 | | | | | | .) | = | 3 | 157,86 | |
| | 7912 | 47,10 | 5 | 39.18 | 24.9 | | | 92,78 | 183 | = | 163.56 | 162,08 | 153,66 | . 88 | 3. | | | | | 161,58 | | 3 | = | Z, | | | 150 051 | 59.86 | | | | 9 | | = | 3 | = | - 1 | | |
| | | 8. | | • | 2; | | j | 3 | ES. | 116,08 | | 5 | _ | = | - | | | | 157,00 | 35.8 | | 153,04 | 133,8 | | | | | 2 | | i. | 127 | 130 130 130 | 156.00 | 154,81 | 157.86 | R. /c! | | 2 9 | |
| | 2164 | 175,20 | | | 161.40 | | 174.06 | 166. | CS | 114, 80 | 167,88 | E 59 | 136,66 | 3 | 3 | | 20 | 12551 | 161,00 | 164,46 | 5 | - | | | 4 | 35 | ١. | | ,,, | | | _ | _ | ~ . | | | 4~ | | |
| | EIZA | 87.83 | 1 | 4.28 | 7 | j | 33,10 | | C124 | 126,98 | • | | | 166,28 | 165.00 | | 7 7 7 | 3 | . 66 | 3 | 154,48 | 162,78 | 102,00 | 132. | 200 | 165,28 | 163,50 | 164,58 | | | | 157,06 | | | | 707 | | | |
| | CH | 141.46 | - | | 100 | | 148,39 | 5.73 | E . | 114,00 | 164,90 | 162,13 | 152,48 | 159,64 | 157 | | 79 | 201 | 161.00 | 161,78 | 155,00 | 157.68 | 20 001 | 109 | 10.55 | 168.48 | 151.86 | 161.86 | 188 70 | 7 | 151.00 | 151,30 | 154.00 | 151.00 | | | 152.58 | 155,96 | |
| | 8134 | 22,38 | 1 | 11.48 | 7. | | 53,66 | 26.98 | CSK | 3 . | 100 | 191 | | wi | • | | | 1 | 156,86 | 154,48 | | | | •. | | 156.98 | 157.00 | 153, 88 | . 24. | | 152, 88 | = | | | | | al i | N | |
| | 8144 | 93.5 | | | 76. | | ., | | CEN | 3 . | 152,58 | - | 145,88 | | | | į | | 153,06 | 350,00 | | | | | | 100 | | _ | ,67 | | 140 | | = | | | | 'n | 138,00 | |
| | 8144 | 3. | | 3 | 125,56 | 25.00 | 146.88 | | C2M | ₹. | 155,88 | 135,06 | 145,88 | 90, | 153,78 | | 156.88 | | 13 | 144.89 | ŀ | 3 | | 120.15 | 28. | 155.68 | 57. | | 44. | | 143 | • | = | | 2 | - | 155.88 | | |
| | N 10 | | | | 124.16 | a . | 158.66 | 146.68 | CIN | 126.00 | 165,79 | 155,88 | 144.88 | 154,66 | 6 | 2 | | 3 | 146.38 | 147,18 | 138,08 | 138.58 | 12,5 | 12/21 | 37 | 142.28 | 143.86 | | . 44 BE | | 146.68 | 134.00 | 134.0 | 143.8 | : : | | 145 | 148.88 | |
| | ACC. | 23 | | 2 | = (| | 1 | ٠. | REC | * | 50 | 9 | 91 | 9 | 2 | 9 4 | n 6 | × | 13 | 17 | 22 | | - 1 | 21 | | 2 4 | - | 8 | • | ١ | | 28 | 12 | z | 12 | | 4= | ;= | |
| _ | 12 | 195989 | 10000 | 10000 | 236888 | 2000 | 898439 | ₹ 2 | | 616819 | 867888 | 111501 | 986888 | 816219 | 898523 | 92920 | 10000 | 20000 | 888438 | 305888 | 1012 | 888519 | 12588 | 969181 | | | 818913 | | 2777 | | 846516 | 615889 | 11523 | 819619 | 119200 | 79949 | E44915 | 838917 | |
| H POSITION | HISSION | 5847 | 4/80 | 1811 | 6782 | 17.78 | 3612 | 2086 88 843103 POSITIO | HTSSIOK | \$101 | 2013 | 4785 | 2388 | 1815 | 5914 | 6186 | | | 3812 | 4786 | 2886 | 9101 | 2782 | 5428 | | 67.83 | 78/9 | 3784 | e i e | 1 | 2838 | 1815 | 5814 | 101 | 212 | | 6784 | 3784 | |
| | | S | | 16 | | | ~ | 3427 | <u> </u> | ~ | 38 | l | | | | | | | ŝ | | | | | | | | | | • | | | | | | | | | | |

on and other planting on

TABLE B-2 (Continued)

PEAK OR NAXIMUM RMS LEVELS PRODUCED BY TRANSIENT FLIGHT CONDITIONS LISTED IN TABLE 4

| I | 3417CH - POSITION | 71045 | - | | | | | | | | | | | | |
|----|-------------------|---|----------|--------|-------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| ۳ | NTESTON | DATE | 12 | CIN | C2 % | CEN | CSH | 165 | CISH | H90 | 25 | 5 | E2H | CIEN | CIIX |
| 7 | 2013 | 195991 | 22 | 143,00 | 142.48 | 134,96 | 145,00 | 142.00 | | 145.00 | 142,00 | 145.49 | 144.00 | 144,00 | 134.00 |
| 7 | Ziei | 808428 | 2 | 127.68 | 125,08 | 127.88 | 127,00 | 138,66 | 149.00 | 137,00 | 137.8 | 130.06 | 139,14 | 136.86 | 147,90 |
| 10 | TE MISSION DA | DATE | . 22 | 6174 | 7113 | C194 | C24A | 144 | ESA | C284 | EI | C214 | H71 | CZZA | 5234 |
| - | 1 | 915306 | ٠. | 7, | R. | 18 | 5: | 35. | | | 30,00 | | | 30.3 | 3 |
| | 2315 | 533628 | - | , A | 22 | 77 | 3 | | a. | 35 | 134,28 | 27 | | 3 | = |
| | - | 829628 | • | 41 | •26 | | .54 | 6 | 52 | | 32.58 | 12. | | -83 | = |
| 4 | 1811 | 889888 | ~ | 1,16 | 65, | 38 | . 84 | | 1.12 | | 41.00 | 25 | 121,36 | 181 | 3 |
| | 5312 | 365626 | n - | | : : | 7. | 27 | 1.9 | 7. | 75. | 132,30 | | 132,38 | ai 1 | ¥; |
| | 4123 | 816248 | - | 88 | | 1,96 | | 1.5 | 20.5 | 1 | 124.30 | | 135.78 | is. | F |
| 50 | 4823 | 116111 | S | 79. | 62. | 1:34 | 57. | 1.68 | 3. | 3,88 | 122,98 | 1.28 | 129,00 | .32 | .72 |
| • | 1816 | 615988 | 22 | 2.28 | 1.73 | 1.71 | 3,58 | 5.28 | 4.4 | 1,6 | 3. | 1.8 | 144,00 | 2.3 | |
| 21 | 5115 | 888628 | R | 2.98 | 1.1 | 2,80 | 3,78 | 3.96 | 3.70 | S,98 | 133,09 | 2,48 | 145,66 | 2,50 | • |
| i: | 2866 | 888513 | 22 | 2,38 | 1.78 | 1.88 | 2,48 | 11.00 | 3.78 | 1.23 | = | 1.69 | 149,80 | 1.96 | 6,28 |
| 18 | 3813 | 119868 | 2 | 3.60 | 3. | 71. | 2.78 | 1.16 | 6. | 1 16. | 140,88 | S. | 141,60 | 1.86 | = |
| 28 | 3623 | | 17 | 98.9 | 5,00 | 93.0 | 1 | 12,00 | 6.28 | 1. | 150,06 | 9.0 | 142,56 | | 3. |
| | 22.5 | 101201 101501 | ٦. | | 10.9 | 2 2 2 | - | 86.71 | 2 | | 136.36 | 22. | 155 | 2 | |
| | 1815 | E 1519 | 41 57 | 4 | = | 3, | | | 8 | - | 156,78 | 7.7 | 153.94 | 2 | |
| | 2014 | 560523 | 2: | 7. | 5.00 | 3 | | 25.01 | 6,53 | 2 | 96, 86 | 9.5 | 153,00 | 8°5 | 2 |
| | 1811 | 00000 | 7~ | 2.38 | | | | = | 2.5 | ~} | | 2 | 200 | 2 5 | |
| | 100 | | 4 | 3.86 | 5.88 | 6, 83 | _ | 5.58 | 3.06 | , | 146.60 | 1.29 | | 6.43 | |
| 39 | 5813 | | 13 | 4,46 | 5.86 | 7,11 | 8,24 | 13,00 | 5.00 | | 155,00 | | 149.86 | 2 | = |
| | 4785 | 111111111111111111111111111111111111111 | <u> </u> | 7.5 | 7. | | , . | 98.6 | 7. | 3,7 | 36.161 | | 159.86 | 5.86 | 16,78 |
| | 5326 | 989888 | 2 | 3.28 | | 200 | 5.28 | 8 | 1.00 | | 157.78 | 5.28 | 120,54 | 7.78 | 2 |
| | 3213 | BBF611 | = | 2, 58 | 27.28 | 2.68 | = | 2 | 7- | 되 | 145.88 | = | 144.00 | 뷬 | = |

TABLE 8-2 (Continued)

PEAK OR MAXIMUM RMS LEVELS PRODUCED BY TRANSIENT FLIGHT CONDITIONS LISTED IN TABLE 4

| 4623 | 2 | | 2 | 2 | = | | #. E | | 7,7 | | 1.30 | ; | 7 | 3.56 | | = | Į, | | | 1 | 3. | | | | | Ę | 1 | • | Ļ | | 1.06 | 3 | 1 | | |
|------------------|-----------|----------|------------|--------|---|------|--------------|--------|----------|----------|---|-------|-------------|--------|---------|--------|--------|-------|---------|-------------|---------|-------|----|--------|--------|-------|--------|---------|--------|--------|--------|--------|--------|-------------|-------|
| 7227 | - 1 | 2: | | | | | 1. | | Ŗ: | | 3 | | 32 | y | | 2,50 | 2,38 | | | Ė | 112 | | À. | | n N | 12. | | | 2 | 22 | 11 | ** | 1 | 2 | |
| 84 H | 1 | 145,98 | 1 | | 1 | 1 | 140,00 | | 149.20 | 2 | 98.97 | | 163,38 | 2 | 101101 | 143,66 | 146,58 | , | | 0134 | | | 2 | 22 | .27 | 7 | . | 7. | 49. | 7 | -28 | | 3 | 12. | |
| 5214 | 73 88" | 71 88 7 | 20 2 | | 1 | | 1,30 14 | | 7. 49 1. | | 7. 06.7 | | 2.98 5 | | 1 12 1 | 1,61 | | | | 790 | | | 1. | 827 | .32 | 12. | | • | 1.1 | 98 | . 48 | | | .75 | |
| E1# | Ę | 1 | 152,46 | | | | | | 123,00 | 1 | | 200 | 62.59 | | 24.5 | 77 | 746.00 | | | 110 | | | 2 | .28 | .21 | 3 | | ** | .29 | | . 13 | ! | | 25 | |
| 1823 | V. ee 151 | 3. 25 15 | 5.86 15 | 7 7 | | | 4. 28 155,20 | | 14,10 12 | 21.09.22 | *************************************** | 1 | 6,78 126,19 | | 27.48 1 | 5 | ďΣ | • | | 120 | | 1. | 35 | Ç | 57. | 6 | : | ē. | 1.28 | | 7. | | 3 | | |
| 193 | | 1 | | | 1 | 1,10 | 88.3 | 1 | ì | 3 | 1 | 2 | 3.26 | 1 | 18.48 | | | Z. | | 1110 | | Ę | = | | 99. | | Z . Z | 2,48 | 1.42 | 8 | | | 5 | \$ | |
| 779 | | | | | 1 | | 1 | 18.00 | 1 | 0.91 | | | . 70 | 1 | 11.36 | 1 | 1.5 | 2.4 | | 7930 | | • | | , , | 12: | | ī. | .30 | | 52 | | 034 | 24 | 3 | 1 |
| 1763 | • | | - | 1 | 1 | | -1 | | 1 | 7 | 1 | 1,28 | • | | 2.91 | | 2,68 | 1.7 | | 67.4 | | 10, | | N. | SS. | | 7. | 67. | | , N | : | | .= | | |
| | | | | 1 | | 1 | Į | 9, es | ١ | | | 3, 88 | | 2 | 36,3 | l | 1.30 | 1.60 | | 700 | į | 118 | | S, | 50 | | .37 | i. | | 1 | | | . 23 | 74. | |
| 1 | • | | 2 : | 1 | | 19.0 | - | 4,88 | 1 | 2,81 | ١ | 2,38 | | 5 | * | | 17.48 | 1.66 | | | 700 | 12. | | 72 | | | E, | .42 | | 2.5 | 96 | 46 | 3 | ; | |
| : { | C174 C | | 2,48 4. | | | l | | 7 88 7 | | 2.28 | ١ | 1 | 1 | | | 1 | 73.5 | 1.5 | | | 170 | 11. | | .22 | 92. | | ,28 | 48 | | 1.26 | 21. | 35 | | | = |
| • | | . E. | | ١ | | | | | | | 9 | | | | | 1 | | 12 | | | יננ | - | • | 5 | 4 | N | 2 | 3 | 87 | 2. | = | 9 | * | } } } | |
| | DATE REC | | ı | 386 | | اه | 110999 | ì | | 188817 | 898917 | | 386917 | 916988 | | 12891E | | 15005 | 78. 18 | • | DATE C | ABARB | | 648513 | 611659 | 31935 | 886519 | 4 1 4 1 | 416440 | 868898 | 899623 | 195949 | 71,000 | | 86628 |
| SALTCH POSITIONS | HISSICH D | | 7146 | • | 1 | ١ | 2012 | -1 | 2000 | 8 7845 | | 1 | 3764 | 7823 | l | 4123 | | 2115 | POSTTAR | | H135108 | | | 20.26 | | | 1815 | - 1 | 3131 | 2013 | į | 98.47 | | 200 | 5812 |
| 34I1CH | TC HT\$ | | | | | | | 1 | 7 | | 7 | | 25 | 3 | S | 3 | | 2 | | | THE THE | | -1 | 1 | • | | - | , | 2 | = | , | 1 | | | 2 |

TABLE B-2 (Concluded)

我看到我的时候,只有你只是一种说话,只想你就是我就是一个人的话,我也不是一个人的话,也不是一个人的话,也不是一个人的话,也是一个人的话,也是一个人的话,也是一个人

PEAK OR MAXIMUM RMS LEVELS PRODUCED BY TRANSIENT FLIGHT CONDITIONS LISTED IN TABLE 4

SKITCH FOSITION, 11

| 1481 | 2,00 | 2 | 2,06 | H, | 2.5 | = | 7.00 | 1 | | 8124 | 126,68 | = | = | 151,78 | = | : | | | = | 3. |
|---------|--------|-------|-----------|--------|------------------|--------|--------|--------------|----------------|----------|------------------|--------|-------|----------------|--------|-------|--------|--------|----------|--------|
| A474 | .56 | 3 | 25. | 3,06 | 35.6 | 8,7 | 2,56 | 2.18 | | DIAA | ,26 1 | | .2 | 1 95. | 2 | | | 3. | .15 | .23 |
| C281 | = | 1.66 | 2. | 4.50 | 9.36 | 1.78 | 3.00 | 3.38 | | E15A | 12,58 | 13,00 | 15,18 | 31.00 Se.10 | 20,05 | 21.12 | = | 27.18 | 28.98 | 31,94 |
| A52A | 9. | 2. | 2. | | 27.0 | .75 | 9 | 76 | | E36A | 11.0E 15.89 | 12,88 | J | 28.00 | 18.78 | - } | - 1 | 22.18 | 23.64 | 25.78 |
| C264 | = | 3 | = | = | 10,50 | | 3,38 | | | EBA | 2,5 | | .53 | 1,10 | - 1 | 1,00 | - [| 2.00 | 1.18 | 2.76 |
| A51A | 95. | 7. | 8F: | 5. | 1.18 | | . 54 | .73 | | £141 | 11,28 | 15, 86 | 16,91 | 22, 88 | 16,38 | 28.78 | 3. | 19.66 | 28,38 | 28.20 |
| 7977 | 2.01 | 1.43 | =-7 | 5.28 | 12,58 | 16.1 | 8,58 | 1.20 | | EISA | 1.88 | 2,116 | 32 | 17,98 5,88 | 12,01 | 59.86 | 98.89 | 37.23 | 21.28 | 75.68 |
| 1511 | | .67 | = | 3.86 | 2.81 | 3,60 | 2,56 | 2.26 | | £17A | 15, 88 21, 58 | 18, 88 | 17,56 | 38,48 51,88 | 35,50 | , | = | 47.36 | 36.28 | 57.68 |
| C27.4 | 7. | 4.38 | 2,11 | 5,31 | 25,78 | 12,16 | 1,26 | 2,48 | | 123 | 18.98 | 18.88 | 30.0 | 43,88 | 33,68 | 47.33 | = | 39"68 | 32.68 | 38,50 |
| A58A | . 26 | . 122 | 83 | | 1,52 | 1,28 | .76 | 1,13 | | EBA | 9,28 | 10,00 | | 48, 98 | 24,73 | - 1 | = | 36.48 | 36.38 | 29.48 |
| 7677 | | 11. | 91. | 69. | 1.39 | . 87 | 85 | .87 | | Š | 7.85 14.56 | 19.66 | | 27.98 | 24,48 | 5 | = | 99. | 22,78 | 36,58 |
| C25A | .43 | Ľ. | 69 | 3.96 | 95.98 | 9.00 | 3,16 | | | EZA | 11,58 | 15, 89 | | 78.88 | 81.38 | | I. | 58.49 | 76.49 | 106.00 |
| 324 | ** | | 22 | 27 | 5 5 | 22 | 28 | 2 | | REC | e - | 22 | ž | ~ ~ | 22 | ı | 9, | 10 | S | 25 |
| DATE | 815888 | 89666 | 965649 | 615009 | 888438 888623 | 888519 | 886561 | 68662 | | BATE | 888513 | 696523 | | 989938 | 684523 | | 368456 | 868519 | 896623 | 898629 |
| NEISSIN | 2986 | 285 | 2938 | 1816 | 3913 | 1816 | 4786 | 5812 | Saitca positio | HTSSION | 2886 | 5914 | | 2988 | 5014 | - 1 | 2613 | 9181 | 1101 | 2103 |
| 10 | ~ | | 45 | == | 7. | 15 | 97 | 2 | \$#11¢ | <u>1</u> | - | 21 | | - | ** | 27 | 74 | 13 | 9: | 94 |

APPENDIX C

SAMPLE LISTINGS OF TEMPERATURES, FLIGHT PARAMETERS AND OTHER PDAS DATA

| Table C-1 | List of Signals Input to PDAS |
|-----------|--|
| Table C-2 | Sample Listing of Typical Temperature Data |
| Table C-3 | Sample Listing of Typical Flight Parameter Data |
| Table C-4 | Sample Listing of Automatic Gain Control Amplifier Gain Status |

TABLE C-1 LIST OF SIGNAL INPUTS TO PDAS

| Abbreviation | Signal Description |
|---------------------------------|--|
| STABL | Horizontal Stabilator Left |
| STABR | Horizontal Stabilator Right |
| PITCH | Pitch |
| RUD POS RCLL | Rudder Position Roll |
| PITCH R | Pitch Rate |
| MACH | Mach Number |
| EPR L | Engine Pressure Ratio, Left |
| FUEL | Total Fuel Altitude |
| ASP | Airspeed |
| EPR R | Engine Pressure Ratio, Right |
| HDG | Heading |
| SS ANG | Sideslip Angle |
| A/ATT | Angle of Attack |
| N2R | N2 Right-Engine Spool Speed |
| N2L | N2 Left-Engine Spool Speed |
| YAW R | Yaw Rate |
| AY | Lateral Acceleration - Ay |
| RAM T | Ram Air Temperature |
| RAT ROLL R | Ram Air Turbine Excitation Roll Rate |
| AZ | Vertical Acceleration c.g Az |
| SENSE 8B | Air Flow Sensor Temperature 2B |
| FLOW 8B | Air Flow Rate 10/20 |
| DIF PR | Differential Pressure - Never Used |
| GAIN 1 thru GAIN 12 | Gain of AGC Amplifiers 1 thru 12 |
| HUM SENSE HUM ABS PR | Relative Humidity Relative Humidity Temperature Absolute Pressure in Equipment Bay |
| SENS F 18 TC1 thru TC15 | Air Flow Sensor Temperature 1B Thermocouples Numbers 1 thru 15 |
| FLOW F18 | Air Flow Rate 9/14 |
| EVENT | Weapons Switch Off and Weapons Release |
| F FLOW R | Fuel Flow, Right |
| F FLOW L | Fuel Flow, Left |
| STEP | Switch Position |
| ACCEL 1 thru 15 R ST P ST | Flutter Accelerometers 1 thru 15 Roll, Stick Position Pitch, Stick Position |
| IN DAMP | Inboard Damper - Not Used |
| C DAMP | Center Damper - Not Used |
| IN SPOIL OUT SPOIL PED POS | Inboard Spoiler Outboard Spoiler Rudder Pedal Position |
| WNG SWP DEG | Wing Sweep Degrees |

TABLE C-2. SAMPLE LISTING OF TYPICAL TEMPERATURE DATA

| PROJECT. 1472TAGE | | HSN 10119 JUNE 1988 |
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SAMPLE LISTING OF TYPICAL FLIGHT PARAMETER DATA TABLE C-3.

TABLE C-3 (Cont). SAMPLE LISTING OF TYPICAL FLIGHT PARAMETER DATA

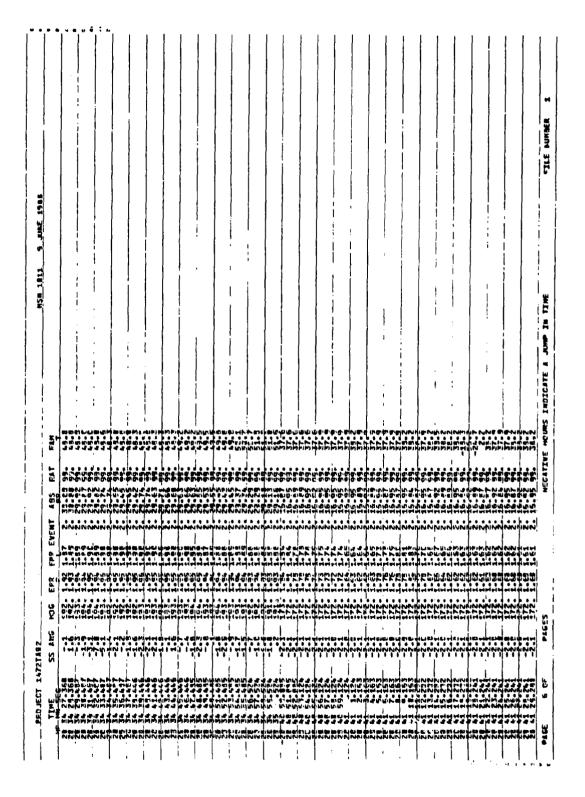
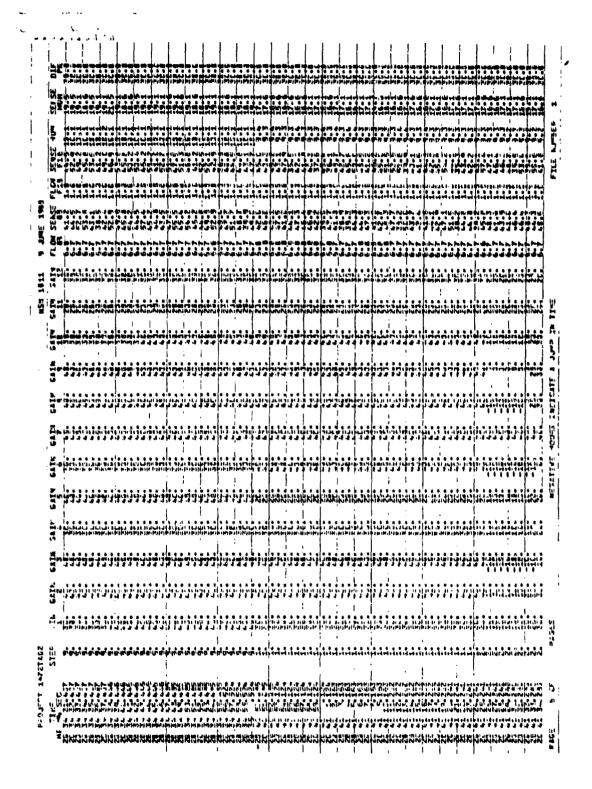


TABLE C-3 (Concluded). SAMPLE LISTING OF TYPICAL FLIGHT PARAMETER DATA

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|--|-------|-----------|------|-------|----------|-------|--------|------|----------|--------|----------|--------|-----------|----------|----------|----------------|-----|--------------|-------|---------|---|--------|--------|--------|-----|-------------|-------|-----------|------|--------------|-------|----------|----------------|-------|-------|--------------|
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| | U | j | 4 | 14 | 1 | - | 1.2 | بلد | 4 | بد | ; | - | 34. | - | | ** | 14. | 2. | 2 | * | 1 | 14. | يدا | | 42 | | 44 | واما | - | والد | 44. | 2.2 | du. | رياد | 1. | 144 |
| | 11 | ف | | | 3 | - | :2 | 4 | . | - | | : | - 47 | - | | | - | *** | ** | - | | | | ن ن | - | | +: | 4: | | 2 | : : | - | . | 4:- | - | * |
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| | ATA. | | | 1 | ï | | | | 7 | - | 1 | | i. | *** | | 7 | | XX. | *** | | 45 | | | 77 | | | | 44 | | 77 | | 77 | ļģ. | 17 | 77 | 17 |
| | PITCH | 797 | | 366 | 121 | 7 | 7 | 7 | - 121 | 200 | | 7 | Ž | 7 | 121 | | ** | 33 | | * | ** | 7 | 7,2 | 12 | 1 | Į. | | 72 | | | Ž. | <u> </u> | | *** | Ŧ | |
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TABLE C-4. SAMPLE LISTING OF AUTOMATIC GAIN CONTROL AMPLIFIER GAIN STATUS



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- 1. Test Directive No. 1472TAO2/9991T498, Support of AFFDL F-111 Vibration/ Acoustic Testing.
- 2. L. L. Shaw, <u>Full Scale Flight Evaluation of Suppression Concepts for Flow Induced Fluctuation Pressures in a Cavity</u>, Flight Dynamics Laboratory, Wright-Patterson AFB OH, AFWAL-IM-81-69-FIBE, 1981.